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November 5, 2004

Arizona Corporation Commission
DOCKETED

NOV - 5 2004

DOCKETED BY

Jim Fisher, Executive Consultant Utilities Division Arizona Corporation Commission 1200 W. Washington St. Phoenix, Arizona 85007

Re:

Johnson Utilities Company - Application for an Extension of its Certificate of Convenience and Necessity (CC&N) Docket No. WS-02987A-04-0288

Dear Mr. Fisher:

Enclosed please find documents responsive to your letter of May 13, 2004. Johnson Utilities Company has also filed an amended legal description for the Merrill portion of the application concurrently with docket control. The enclosed draft CAAG §208 plan amendment, as well as the wastewater and water design reports for Merrill Ranch, encompass the areas contained in the amended legal description.

The documents included herewith to supplement the initial application are as follows:

Attachment 1- Draft CAAG §208 plan amendment.

Attachment 2- Master Wastewater Design Report – Merrill Ranch.

Attachment 3- Master Water Design Report - Merrill Ranch.

Attachment 4- Arizona Department of Water Resources ("ADEQ") Well Identification numbers, nitrate and arsenic concentration for all drinking water wells serving Johnson Utilities Company's water systems.

Attachment 5- Arizona Department of Environmental Quality Public Water System Identification numbers for all drinking water systems serving Johnson Utilities Company.

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Jim Fisher, Executive Consultant November 5, 2004 Page 2

Attachment 6- ADEQ facility numbers for all wastewater treatment plants serving Johnson Utilities Company.

Notably, the enclosed CAAG §208 plan amendment is pending approval. However, there are no water and wastewater facilities that have been constructed within the two proposed certificate extension areas nor will services be provided until such approval is required.

Should you have any questions, please do not hesitate to call. Thank you for your time and efforts in this matter.

Very truly yours,

L. Shapiro

Enclosures

cc: Brian Tompsett, Johnson Utilities Company Docket Control (w/enc.)

1603847.1/51239.003

ATTACHMENT 1

CAAG 208 WATER QUALITY PLAN AMENDMENT FOR MERRILL RANCH FOR JOHNSON UTILITY SERVICE, LLC

November 2004

PREPARED FOR:

JOHNSON UTILITIES COMPANY, LLC

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CAAG 208 WATER QUALITY PLAN AMENDMENT FOR MERRILL RANCH

November 2004

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SECTION 1 – INTRODUCTION

This CAAG 208 Water Quality Plan Amendment will address the expansion of the Merrill Ranch area to the Johnson Utilities Company, LLC service area. The proposed project is located in Pinal County in an area of relatively flat topography. The sites are equally accessible to Phoenix and Tucson metropolitan regions and close to Florence, Apache Junction and Queen Creek. A portion of the Merrill Ranch Development includes the Mystic Lake Ranch area (shown on Exhibit 5a and 5b) as well as area east of Mystic Lake. A portion of the expansion area that is to be added to the Johnson Utility Service area is currently in the expansion of the City of Florence, Arizona 208 service area, however, the City of Florence has requested that Johnson Utilities provide sewer service to the first phase of Merrill Ranch since the city has no facilities in the vicinity of this site. The land within, and surrounding, this projects has historically been used for agricultural purposes. The main objective of this amendment is to propose the development of a wastewater treatment plant site that will serve numerous planned communities. It is anticipated that the project will use all of the reclaimed water produced from the wastewater treatment plant. Merrill Ranch (aka Rancho Sendero or Mystic Lake Ranch)site and its water reclamation facility (WRP) will be addressed in this amendment. Johnson Utilities Company, LLC's service area is located within the project areas and will be providing development, maintenance and operation of the wastewater facilities.

Development regulations serve as the primary mechanism for implementation of the land uses for the four projects. All construction and development within the PAD area shall comply with applicable provisions of the Pinal County Building Code. For the purpose of this PAD, the table in Exhibit 3 lists the types of land uses to be established. The project will contain varying residential densities, a golf course and club house, an elementary school, a high school. A fire station, a worship parcel, 2 recreation areas, and park site.

Merrill Ranch includes Rancho Sendero (Mystic Lake Ranch), a 1758 acre mixed use development, is located in central Pinal County along the east and west sides of Hunt Highway approximately five and one-half miles south of the Johnson Ranch development. Amendment #4, Mystic Lake Ranch

area included 2643 acres, 1051 for Mystic Lake Ranch and 1592 acres for Farley Farms and other undeveloped land between Farley Farms and Mystic Lake Ranch. The Merrill Ranch area is 885 acres less than the Amendment #4 208 Amendment. Hunt Highway makes a 90 degree turn to the east at the southern boundary of the project. The southeast corner of the project is formed by the intersection of Attaway Road and Hunt Highway. The northern part of the project is bounded by the future alignment of Franklin Road, while Felix Road is one mile east of the eastern boundary. The site is surrounded by state, private and agricultural land.

The site will consist of low to medium density housing (Family-3.7 u/a and Active adult-4.2 u/a), a 15-acre elementary school site, a 40-acre high school site, a fire department site, a 16-acre worship site, an 18-hole golf course and clubhouse, 2 recreation sites(17 acres and 20 acres) and three 5-acre park sites. The development will also include an 2 recreation areas, three parks with an extensive trail system, and a riparian preservation area complete with hiking trails. The developer has enlisted the design services of a wildlife consultant to enhance the vegetation and wildlife within the riparian corridors.

Summary:

The proposed plant will be developed as an Aero-Mod Extended Aeration mechanical plant. The Extended Aeration plant is designed to provide seven potential phases of operation, however, the duration and number of phases is based on process considerations related to the effluent quality requirements of the specific wastewater treatment operation. Construction of the Water Reclamation Plant (WRP) and wastewater collection infrastructures will be phased in accordance with the growth and needs of the proposed development. Each future phase of the WRP will be constructed and operational before the capacity of the existing treatment facility is exceeded. The wastewater facilities will be designed to allow orderly expansion to occur as additional capacity is required. The wastewater effluent will be treated to reuse standards, for 100% reuse on open spaces, golf courses, recreational areas and landscaped areas.

The communities can be serviced within a short distance and the profile of the mechanical plant will be constructed to be aesthetically inconspicuous. The plant expansions will allow the facilities to

provide wastewater treatment to adjacent properties providing the parcel is within the utility's approved CC&N, and desires to be served. The main wastewater plant has anticipated growth in their immediate area, and will be sized accordingly.

Development of this project is anticipated to begin between the years 2005 through 2008. The project is composed of one or more of the following: family housing, adult communities, elementary school, high school, recreational areas, golf course and club house, fire station, recreation and park sites.

Johnson Utilities Company, LLC was formed as a utility company and is registered with the Arizona Corporation Commission (ACC) to provide water and sewer service to this area. Due to developer and consumer demand, Johnson Utilities Company, LLC will construct, operate and maintain the WWTP facilities. The franchise for utility service to this area has been granted by Pinal County. These proposed sites are within the currently approved franchise for the utility. Johnson Utilities Company, LLC has a Certificate of Convenience and Necessity (CC&N) from the ACC in order to provide water and wastewater service for the franchised areas, which will include Merrill Ranch. Approval of said application, and pending applications, will grant Johnson Utilities Company, LLC the proper rights and authorities to implement this plan. A copy of the CC&N. is on record with the ACC (Appendix D).

SECTION 2 - MERRILL RANCH

DESCRIPTION OF PROJECT

Merrill Ranch will be developed to incorporate a range of low to medium density single family homes, an elementary school, a high school, an 18-hole golf course and clubhouse, a worship center, 2 recreation areas, 3 parks, trails several commercial areas and community parks connected by an extensive trail system. Riparian areas will be enhanced with hiking trails which will serve as a natural buffer between and within the proposed housing developments. The extensive trail system, recreational areas, and riparian preservation area will provide for approximately 18 percent of open space in the total land area.

It is anticipated that the project will be developed in four major phases (*Exhibit 5b*). The initial phase is a Planned Area Development (PAD) consisting of approximately 362.5 acres and has been approved for approximately 1,523 family units. The golf course, recreation areas, extensive trail system and riparian area will be developed in the latter part of this phase. Phase two consists of 425 acres with approximately 1703 housing units and the elementary school. Phase three consists of 407 acres with approximately 1381 housing units and a riparian area. The final phase of this project covers approximately 314 acres consisting of 1,161 housing units, a high school, a park site, and a trail system.

The WRP will be located in the southern western portion of the project. Treated effluent will be pumped by a reclaimed pump station to the golf course and riparian areas for 100% reuse on turf irrigation, open spaces, and landscaped areas. The initial plant will have a total capacity of approximately 1.0 MGD.

Summary:

The proposed plant will be developed as an Aero-Mod Extended Aeration mechanical plant. The Extended aeration plant is designed to provide several potential phases of operation, however, the duration and number of phases is based on process considerations related to the effluent quality requirements of a specific wastewater treatment operation. Construction of all the water reclamation plant (WRP) and wastewater collection infrastructures will be phased in accordance with the growth and needs of the individual projects. Each future phase of the WRP will be constructed and operational before the capacity of the existing treatment facility is exceeded. The wastewater facilities will be designed to allow orderly expansion to occur as additional capacity is required. The wastewater effluent will be treated to reuse standards, for 100% reuse on open spaces, golf courses, recreational areas and landscaped areas

The communities can be serviced within a short distance and the profile of the mechanical plant will be constructed to be aesthetically inconspicuous. The plant expansions will allow the facilities to provide wastewater treatment to adjacent properties providing the parcel is within the utility's approved CC&N, and desires to be served. The main wastewater plant have anticipated growth in their immediate area, and will be sized accordingly. Areas included in this amendment are only areas currently approved by, or those who have applied for service to, the Arizona Corporation Commission (ACC).

Development of these projects is anticipated to begin between the years 2005 through 2006. All of the projects are composed of one or more of the following: family housing, adult communities, elementary schools, recreational areas, equestrian centers, and some commercial areas.

Johnson Utilities Company, LLC was formed as a utility company and is registered with the Arizona Corporation Commission (ACC) to provide water and sewer service to this area. Due to developer and consumer demand, Johnson Utilities Company will construct, operate and maintain

the WWTP facilities. The franchise for utility service to this area has been granted by Pinal County. These proposed sites are within the currently approved franchise for the utility. Johnson Utilities Company, LLC has a Certificate of Convenience and Necessity (CC&N) from the ACC in order to provide water and wastewater service for the franchised areas, which will include Merrill Ranch and adjacent sites. Approval of said application, and pending applications, will grant Johnson Utilities Company, LLC the proper rights and authorities to implement this plan. A copy of the CC&N. is on record with the ACC (Appendix D).

WATER RECLAMATION PLANT PHASING

In preparing the phasing plans, certain assumptions have been made. These include: 1) the rate of growth for the project remains constant as calculated; 2) the rate of growth of other regional projects used in assessing cumulative impacts on phased infrastructure and services remains constant as calculated; and 3) the market demand for proposed residential product type and mix remains constant throughout the phasing intervals. If the build-out rate internal to projects accelerates or decreases, key infrastructural components may be re-phased.

Merrill Ranch WRP will generally be developed in four phases. A summary of the proposed phasing sequence by planning area is provided below.

PHASE	YEAR	INFRASTRUCTURE CAPACITY
A	2005-2009	Start of Project - Start-up of Aero Mod Mechanical Treatment Plant and Effluent Re-use at the adjacent Golf Course, and wildlife area (1.4 MGD).
В	2009-2014	Addition of a 1.4 MGD Mechanical Treatment Effluent Reuse/Excess Discharge
С	2014-2019	Addition of a 1.4 MGD Mechanical Treatment Effluent Reuse/Excess Discharge
D	2019-2025	Estimated build out of the final 1.4 MGD is anticipated to be completed within the remaining 5 years for 7997 units. There will be no additional hook-ups after the 7997 units. Total build out will be 5.6 MGD, and is dependent on economic development trends over the next 20 years.

Johnson Utilities Company, LLC will collect all wastewater with the completed facilities within the designated communities and deliver it to the proposed wastewater treatment plant site.

The proposed site is located west of Hunt Highway, within the North Half (N ½) of Section 25, Township 4 South, Range 8 East, G&SRM, Pinal County, Arizona. Based on builder projections, the utility has anticipated that this site will be constructed and operating at full capacity within the next 15 years. The Rancho Sendero property (Sections 24 and 25, T4S, R8E) is currently owned by Fox Hunt Properties, an affiliate of Johnson Utilities Co., L.L.C. The remainder of the property within Merrill Ranch is owned by Pulte Homes and Del Webb. Johnson Utilities will purchase and construct the WRP at a total build-out capacity of approximately 5.6 MGD. The facility will also

provide service to undeveloped land south of Merrill Ranch. and other adjacent subdivisions if requested within the Johnson Utilities CC&N areas.

Approximately two-thirds of the property will be impacted by the localized drainage from the buttes located on the north and west of the site. Flows running from east to west coalesce with a major wash located along the eastern portion of the site. The wash conveys water from north to south and drains a portion of the Gila River watershed. The proposed site is not within a 100 year flood zone. Detention of offsite stormwater runoff will be achieved by utilizing golf course basins and turf retention.

The treated effluent will be used for irrigation of the golf course to be constructed at the project. The golf course will be located on the east side of Hunt Highway and is spread throughout Sections 24 of Township 4 South, Range 8 East and Sections 18, and 19 of Township 4 South, Range 9 East.. The project is located entirely within the Pinal A.M.A. The golf course parcel within Section 24, Township 4 South, Range 8 East is owned by Fox Hunt Properties, and the golf course property with Sections 18, and 19, Township 4 South, Range 9 East are owned and will be operated by Pulte Homes and Del Web. Initial irrigation of the golf course at Merrill Ranch will be provided by using existing irrigation wells. When the proposed wastewater treatment facility produces enough reclaimed water, the golf course will be irrigated entirely with the reclaimed water.

This water reclamation plant proposed for Merrill Ranch will bring several benefits to the area:

- Merrill Ranch will feature a range of low to medium-high density neighborhood housing, recreation, (equestrian trails, and a wetlands area), and employment opportunities for the residents of Pinal county. The development will increase the tax base without creating infrastructure costs for the County.
- Merrill Ranch will provide a master planned development with a variety of residential opportunities and some limited local commercial uses. The project will allow the County to continue to grow in a manner compatible with the County's Comprehensive Plan.
- Merrill Ranch is located immediately adjacent to Hunt Highway, a major transportation

corridor, which will allow for the efficient use of the existing transportation infrastructure.

The population projection estimates for permanent and seasonal residents within Census Tract Eight of Pinal county will increase from 7,600to 9,894 from 1995 to 2015 (<u>Pinal County Comprehensive Plan, Area 3</u>, 1998). By the year 2015, 2,832 projected new housing units are required to meet future housing needs within the Census Tract Eight area of Pinal County. These numbers were estimated using historic rural patterns of growth within Pinal County.

Summary:

The proposed plant will provide the following benefits for its respective sites:

- The effluent from the wastewater treatment plant will be required to meet effluent reuse standards for open-access golf courses and other open area facilities located adjacent to the WRP, and to meet reclaimed water requirements, which is equivalent to secondary treatment and disinfection. Due to the quality of the treated effluent, the areas of re-use will provide recreational opportunities to residents. In addition, effluent discharged to the waters of the U.S. through a NPDES Permit will be required if all effluent is not used on the golf courses and open space areas. A NPDES permit will be required for this project.
- A higher level of wastewater treatment will be provided, thus eliminating the potential for groundwater contamination from overuse of septic tanks and leach fields in the area.
- The existence of the wastewater treatment plants will allow the areas to accommodate growth without creating detrimental environmental situations due to a lack of infrastructure.
- The project is close to Florence and East Mesa and provide a reasonable commute that will provide housing opportunities to satisfy current housing shortages.
- Affordable housing for prison employees in Florence.
- The employment opportunities in the southeast valley area are increasing with the
 development of Williams Gateway Airport and other significant employers. The
 development will provide housing opportunities for the increased workforce needed.
- The residents of the development will add to the consumer tax base in the existing Pinal County area. The increase in the number of consumers will support growth of commercial

development in Pinal County as well as increased sales tax revenues.

Landscaped open area parks and corridors throughout the development, irrigated with properly treated effluent, will encourage and enhance outdoor recreational activities, which may include golf courses, public parks and lakes, wetlands, and hiking and extensive trail system for the residents within the respective areas.

WASTEWATER FLOW PROJECTIONS

The following is an estimate of the wastewater flows projected for each plant site and the subdivisions it will provide service to. A more detailed flow breakdown by subdivision can be found in Appendix E, Sewer Flow Projections. If the Flow Projection chart is not available for the specific subdivision, it means the subdivision is still in the development stage and no current PAD has been completed at this writing.

Phase A of the sewage flows to this site consists of an initial 1,523 residential units, Phase B consists of 1,703 residential units, Phase C adds another 1,381 residential units, and Phase D incorporates the final 1,161 residential units.

Summary:

In order to estimate the projected sewer flows for these areas of the Johnson Utilities service area, the criteria as outlined below was utilized. Flow estimates for family and adult retirement residential, commercial and school facilities were derived based upon historic flows near this area. The flows are based on the population and acreage per phase of each project. These flow projections have recently been accepted by ADEQ for this area of the valley (See Appendix E). The design criteria for the Johnson Utilities Company is as follows:

SEWER PLANNING CRITERIA

- 90 Gallons Per Capita per Day (GPCD) for all residential areas requiring sewers
- 1.8 persons/Dwelling Units (DU) for all Adult Community Residences
- 2.6 persons/DU for all Family Community Residences
- 1,000 Gallons Per Area Development (GPAD) for all commercial and school areas [Average Daily Flow (ADF)]
- 3.0 Peaking Factor for all commercial and school areas [Peak Dry Weather Factor (PDWF)]
- 250 GPAD for wet weather flow infiltration

WASTEWATER SYSTEM INFRASTRUCTURE REQUIREMENTS

Merrill Ranch will be primarily served by gravity sewer mains. The gravity sewer main sizes have been determined and designed (See Exhibit 6). The proposed lift station pumps will convey the collected wastewater to the wastewater treatment plant site located in the north half of Section 25, Township 4 South, Range 8 East G&SRM.

The wastewater will be treated to Class A reclaimed water standards. The treated effluent will be pumped by a reclaimed pump station to the golf course for turf irrigation and the habitat areas for plantings. Detention of offsite stormwater runoff will be achieved by utilizing golf course basins and turf retention. Basins will be used to intercept onsite stormwater runoff.

Summary:

The water reclamation facility will be primarily served by gravity sewer mains where possible and a force main where needed. The sewer lift stations will lift all flows from the gravity sewer collection system into the headworks of the treatment plant facility. The influent sewer lift stations will be

constructed and upgraded to match the capacity increments of the future wastewater treatment plants as required. The sewer lift stations will be designed using duplex pumps, backup power, and all required facilities to meet ADEQ Bulletin 11 design standards. The actual timing and sizing of the wastewater collection systems will depend on phased construction of the projects. The wastewater generation estimates for family and adult residential and commercial uses were derived based on historic flows near these areas.

Historically, the land in these areas has been used for farming or cattle operations and there have been water quality problems in the past. Houses in this area have treated wastewater by using individual septic tanks. To prevent future nitrate problems, Johnson Utilities will not approve septic tanks, except for existing or previously approved septic tank systems for developments within the Johnson Utilities service area. By providing a high level of wastewater treatment and quality control methods, Johnson Utilities will work improve the quality of the groundwater in this area.

The treatment plant facility will be sized to treat the average daily flow (ADF) and accept peak wet weather flows (PWWF) without disrupting the treatment plant process. The wastewater will be treated to "open access" reuse standards. The treated effluent will be pumped by a reclaimed pump station to the planned reuse areas for the four project sites for golf courses, parks, greenbelts and other turf irrigation. The utilities will be requesting reuse permits approved by ADEQ for the water reclamation facility site to irrigate at a average rate of 5.6 MGD, based on the development project area.

SECTION 3 - WATER RECLAMATION PLANT DESCRIPTION

Exhibit 7, Water Reclamation Plant Site Layout, shows the general layout. The plant will be constructed and phased per service needs as the project develops. Phase A of all the facilities will typically consist of an influent pump station, inlet headworks, and a Aero-Mod Extended Aeration mechanical Water Reclamation Plant having an initial capacity of 1.4 MGD. During the initial phase, the volume of effluent generated will be less than the reuse area requirements. This will be supplemented with groundwater until the volume of effluent meets the golf course requirement and/or turf irrigation needs. Phase B of the mechanical treatment facilities will consist of project phasing as discussed in the Water Reclamation Plant Phasing section.

Johnson Utilities has initiated and anticipated financial requirements for the construction of the mechanical plants in anticipation of developers needs for these areas. The utility has committed to installing the mechanical plants at the proposed sites as soon as permitted. Johnson Utilities will construct the plants. All of the plants are anticipated to be operational by 2005 at the latest.

The developer is integrating the recreational areas, such as golf courses, wetlands, parks and recreational lakes, for all sites into the layout for homes, therefore the areas will not be fenced and the reuse effluent will meet open access requirements. If excess flows are experienced during portions of the winter months, effluent will be stored within the golf course lakes, wetlands, manmade lakes, or used on landscape areas within the community. Effluent discharges into the waters of the United States is not anticipated.

SECTION 4 - PERMITTING REQUIREMENTS

The following is a summary of the permitting requirements and processes that are required for the wastewater treatment plant facilities. Each project will require an Individual Aquifer Protection Permits (APP).

A. Aquifer Protection Permit (APP)

The State Aquifer Protection Permit (APP) Program was established by the Environmental Quality Act (EQA) and is primarily designed to regulate facilities that may discharge to the aquifer. Proof of Best Available Demonstration Control Technology (BADCT) is required. Achievement of BADCT for a wastewater treatment plant facility is outlined in the AAC Title 18. Chapter 9, Article 2, Part B. APP permits will be applied for starting in 2005. This plant will generate the maximum effluent re-use flow permitted by each permit.

B. Reclaimed Water Permit

Each end user will need to obtain a Reclaimed Water Permit from the Arizona Department of Environmental Quality. A copy of any Reclaimed Water Permits will be included in the Appendix A. Modifications to these permits will be made as required. If all of the reclaimed water is not able to be used on landscaping and golf course areas, impoundments (recharge basins) will be necessary for discharging any excess reclaimed water. The reclaimed water will receive ultraviolet disinfection prior to discharging into basins.

C. Section 208 Plan Amendment

In accordance with Section 208 of the Clean Water Act, an Area Wide Water Quality Management Plan was prepared for the Central Arizona Association of Governments (CAAG). The Water Quality Management Plan has continually been updated through several Plan Amendments and updates. This document will serve as the 208 Water Quality

Plan Amendment for Merrill Ranch. The facility will be serviced and managed by Johnson Utilities Company, L.L.C. The Central Arizona Association of Governments (CAAG) is a Designated Area-wide Water Quality Management Planning Agency for Pinal and Gila Counties.

D. National Pollution Discharge Elimination System Permit (NPDES)

A NPDES permit is required for wastewater effluent planned to be discharged to surface waters of the United States. A NPDES Permit for effluent discharges to the waters of the United States is not anticipated to be required for these projects.

A pre-treatment program will be established in conformance with the Clean Water Act (CWA) for non-domestic wastes. The pre-treatment program will consist of chlorination and de-chlorination of effluent prior to discharge which will determine which non-domestic users should be regulated.

The NPDES program also regulates sewage sludge under Section 405 of the Clean Water Act (CWA). Part 503 in the Clean Water Act (CWA) controls the quality of sewage sludge that may be applied to land, distributed and marketed, placed in a sludge disposal facility, or fired in a sewage sludge incinerator. The sludge generated at the proposed wastewater treatment plant will be disposed of at an operating landfill certified by the state to handle and dispose of sludge from wastewater treatment plants. Protection of the groundwater at the landfill location will be provided by the landfill facilities. The closest landfill which can accept sludge for disposal is:

Butterfield Station Municipal Solid Waste Landfill 99th Avenue, one mile north of Highway 238 Mobile, Arizona

Operated by:

Waste Management, Inc. 2425 South 40th Street Phoenix, Arizona 85034 Phone: (602) 256-0630

In discussions with Waste Management, Inc., they anticipate having sufficient disposal capacity to handle the disposal needs of the region for the next 50 years. A NPDES Permit for sludge disposal will not be required by the utility.

A NPDES Stormwater Pollution Prevention Permit will be required for the treatment plant site work. The contractor for the facilities is responsible to obey all NPDES Permit regulations as they apply to construction sites and potential surface water and groundwater contamination. All hazardous materials and potential pollutants shall be stored onsite in appropriate storage areas which are constructed to contain any spills or runoff of hazardous materials. Appropriate sites are to be provided for the washing of construction equipment and capture of the runoff. Retention basins, silt traps, and other sediment barriers are to be provided at the site to filter sediment from storm runoff leaving the site. The contractor shall keep the site clean and have covered dumpsters onsite which are emptied on a regular basis.

E. Wastewater System Technical Review

The technical review process consists of submitting a design report and detailed construction plans for the plant site, treatment plant design, required plant details and associated facilities. The plans will be prepared to be in conformance with AAC Title 18, Chapter 9, Article 2, Part B, as issued by the Arizona Department of Environmental Quality.

F. Local Floodplain and Drainage Regulations

The Merrill Ranch site, when entirely built out, is designed to discharge runoff at a rate equal to or less than the current runoff rate as undeveloped property. The drainage concept for the Merrill Ranch requires that all runoff be directed toward retention/detention basins within the golf course or designated sites. Runoff will be stored in the basins, allowing sediment to settle out, and then be released into the natural drainage courses in a controlled manner. This type of retention/detention drainage concept will be utilized within the four proposed WWTP sites. The retention basins will be landscaped in such a way as to provide bio-filtration of the first-flush storm runoff. In order to eliminate non-point discharges from the golf courses, the golf courses have been designed to retain runoff within swales built into the fairways.

SECTION 5 - PROJECT FINANCING

The cost for wastewater treatment plant facilities will be provided in part through line extension agreements between the developers and Johnson Utilities, and connection fees. The Company was formed as an Arizona limited liability company and has been approved by the Arizona Corporation Commission (ACC) to provide Certificates of Convenience and Necessity (CC&N) for water and wastewater service to this development. As a public service corporation, the Company is required to obtain prior approval of all long-term financing pursuant to A.R.S. 40-301 et.seq.

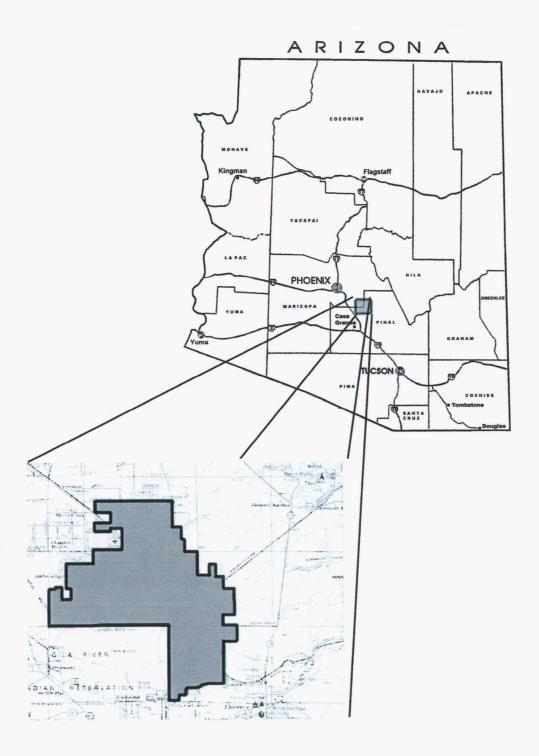
The long-term debt and the managing membership funds will be provided by the Utility, who is serving this project. The associate membership funds will be provided by substantial homebuilders who acquire given subdivisions within the development and who will also pay the costs associated with the utility facilities for that subdivision as part of the acquisition cost. Developer payments will cover all costs for onsite facilities, plus a portion of the common facilities needed to serve that subdivision. These expenses will be funded through the Corporation Commission's tariff, docket # U-2987, approved by decision #60223, on May 30, 1997. This public document is on file with the Corporation Commission.

Cost estimates for the WRP development are provided on Exhibit 9. The estimate is based on a 1.4 Million gallon per day (MGD) Aero-Mod Extended Aeration plant. The proposed plant will be constructed in four phases, each phase will be 1.4 MGD. Construction of additional phases will be required based on the development schedule within the PAD and service area.

As a condition of the Certificate of Convenience and Necessity, the Commission has established the rates at which the Company can charge customers for provisions of the utility services. Those rates include all pro forma costs associated with the operation and maintenance of the wastewater facilities. As operating costs change over the years, the Company will apply to the Commission for adjustments in those rates to cover all operation and maintenance expenses as well as a return on the investment the Company has made in the utility facilities.

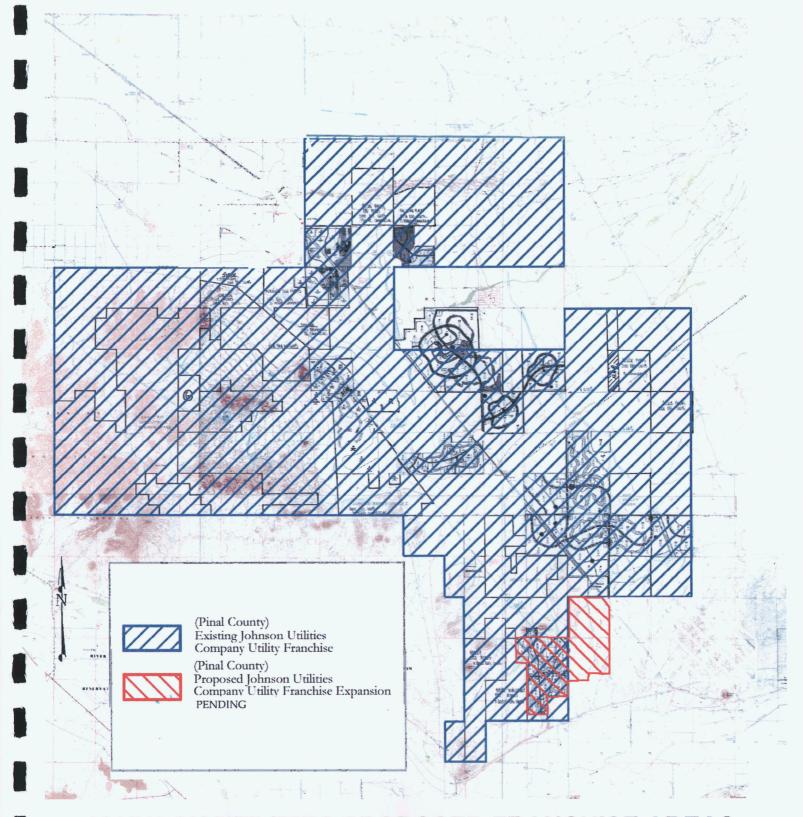
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EXHIBIT 6	MERRILL RANCH MASTER SEWER SYSTEM LAYOUT
EXHIBIT 7	TYPICAL WATER RECLAMTION PLANT SITE LAYOUT
EXHIBIT 8	TYPICAL TREATMENT PROCESS DIAGRAM
EVITDIT 0	DDEL DAINADY CONCEDITON ECTIMATE



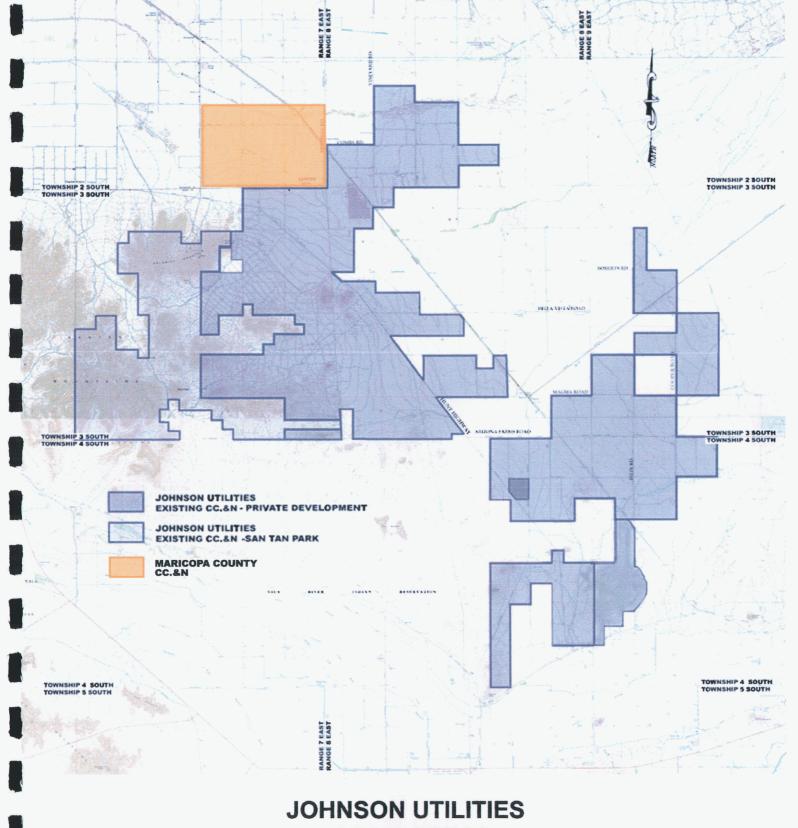
LOCATION MAP

Exhibit 1



JOHNSON UTILITIES PROPOSED FRANCHISE AREAS MERRILL RANCH

208 Plan Amendment #8
Exhibit 2



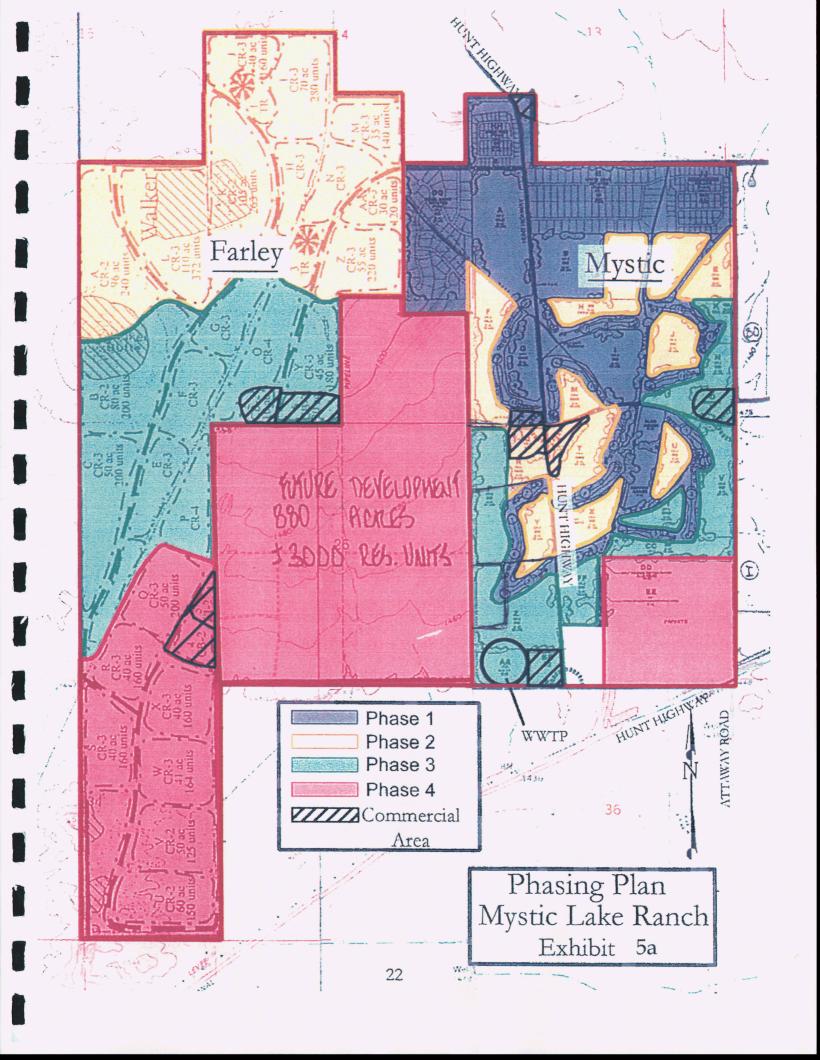
JOHNSON UTILITIES CC&N AREAS PINAL COUNTY

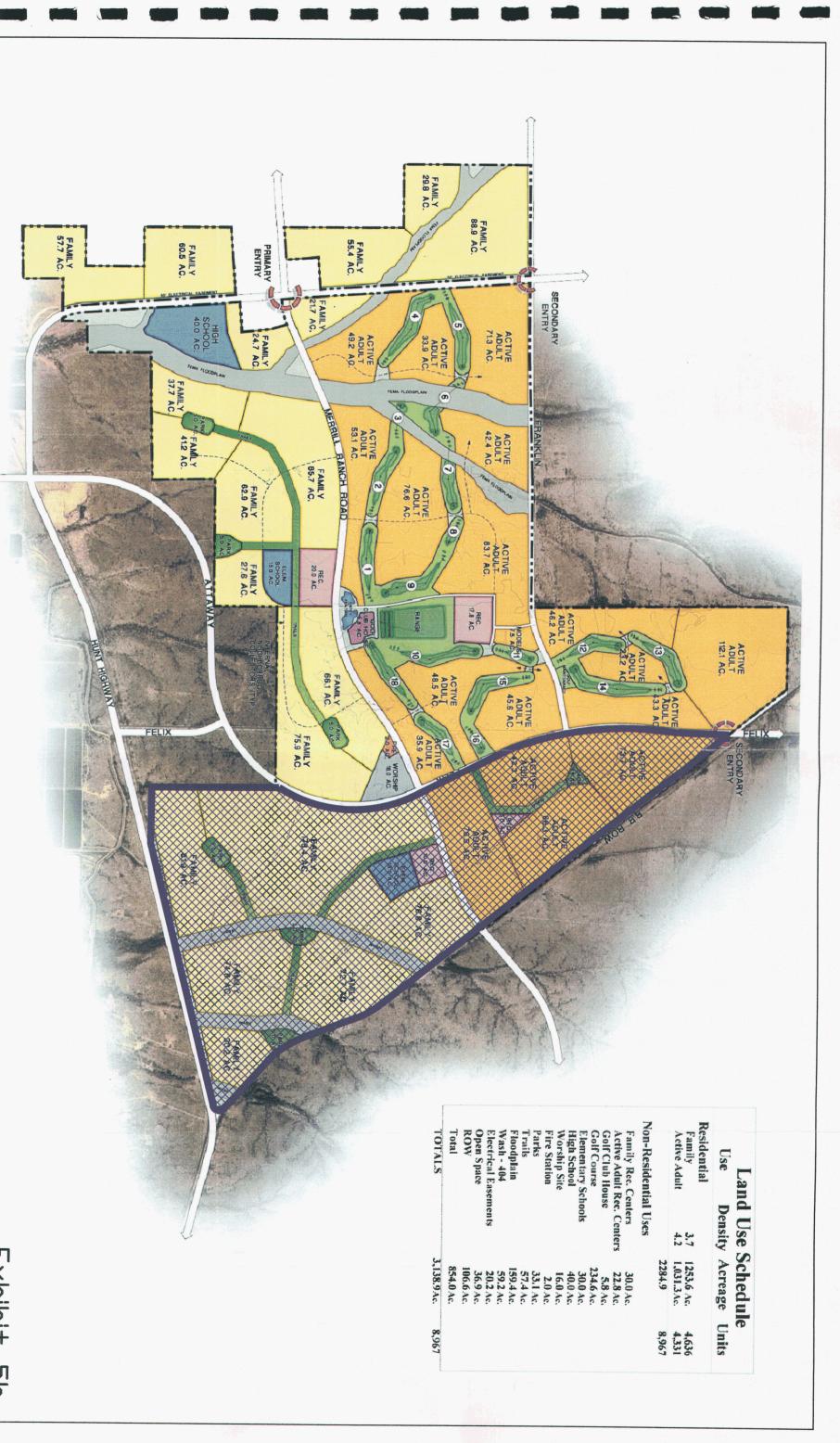
Exhibit 3

LAND USE TABLE							
Residential	Low Density Residential	R-1	3.7	2721.0			
Residential	Medium Density	R-2	4.2	3047.0			
Fire Station	Fire Station	CR-3	4.1 - 7.0	5.6			
Church	Worship sites	C-2		16.0			
School	Elementary School	C-2		15.0			
School	High School	C-2		40.0			
Commercial	Commercial	C-2		6.8			
Parks	Park sites	os		15.0			
Recreation	Recreation Area			37.8			
Golf	Golf	os		234.6			
Riparian Area	404 and wash	os		91.0			

LAND USE TABLE

EXHIBIT 4





PULTE / DEL WEBB

Base mapping compiled from bost available informa All map data should be considered as proliminary, in need of verification, and subject to change File 1:2428141 Conceptual MPIRVI-Con E2 dwp

CONCEPTUAL MASTER PLAN E2

MERRILL

RANCH

Florence,

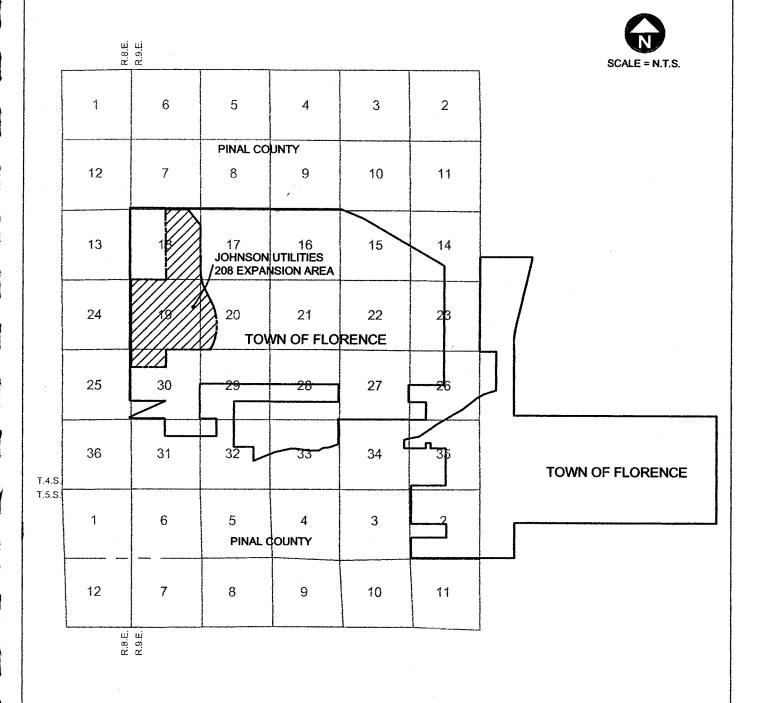
The developer has reserved the right, without notice, to make charges to this map and other aspects of the development to earnfy with governmental requirements and to fulfill its marketing objective.

800

SCALE : 1' - 800'

- 800 NORTH

PULTE-MERRILL RANCH TOWN OF FLORENCE





JACK JOHNSON COMPANY

Designing World Destinations
In-Person - 1777 Sun Peak Drive - Park City - Utah 84088
Tolephone - 435 645 900 - Prepaivale - 435 648 1620
www.designings.co.



PULTE-MERRILL RANCH Legal Description Johnson Utilities-Expanded 208 Area

August 30, 2004

A portion of land lying within Section 19, and portions of Sections 18, 20 and 30, Township 4 South, Range 9 East of the GILA and SALT RIVER MERIDIAN, County of Pinal, Arizona, more particularly described as follows:

Beginning at the found U.S. G.L.O. 21/2" Brass Cap at the North Quarter Corner of said Section 18;

Thence South 89°56'54" East along the Northerly Section Line of said Section 18, a distance of 1705.71 Feet to a point on the Southeasterly Railroad right of way line.

Thence South 39°07'29" East along said right of way line a distance of 1480.55 to the Centerline intersection of Felix Road.

Thence along said Felix Road centerline the following (4) courses.

- 1. South 00°34'05" East 3478.49 Feet to the beginning of a tangent curve, concave to the left and having a radius of 3000.00 Feet.
- 2. Thence Southeasterly along the arc of said curve through a central angel of 27°13'48" 1425.76 Feet to a point of tangency.
- 3. Thence South 27°47'53" East 969.69 Feet to the beginning of a tangent curve concave to right and having a radius of 4000.00 Feet.
- 4. Thence Southerly along the arc of said curve through a central angle of 55°24'15" a distance of 3867.95 Feet to a point of non tangency also being the point of intersection of the centerline of Felix Road and the Northerly Line of said Section 29.

Y:\742MerrillRanch\04_Design\Survey\742 - Johnson Utilities 208 Expansion 8-30-04.doc

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Thence South 89°54'02" West, along the Northerly Line of said Section 29, a distance of 775.03 Feet to a found 3" Pinal County Highway Department Aluminum Cap at the SOUTHEAST Section Comer of said Section 19;

Thence North 89°55'22" West along the Southerly Section Line of said Section 19, a distance of 2622.99 Feet to a found US GLO 2 1/2" Brass Cap at the Quarter Corner point common to said Sections 30 and 19.

Thence South 00°03'30" West along the North-South Mid Section Line a distance of 1321.64 Feet

Thence North 89°55'37" West a distance of 2636.01 Feet to along the South Line of the North half of the Northwest Quarter of said Section 30.

Thence North 00°26'55" West along the West Section Line of said Section 30 a distance of 1322.38 Feet to a found US GLO 2 1/2" Brass Cap at the Northwest Section Corner of said Section 30.

Thence North 00°26'07" West along the Westerly Section Line of said Section 19 a distance of 2646.78 Feet to a found 3" Aluminum Cap at the West Quarter Corner of said Section 19.

Thence continuing North 00°26'00" West along the Westerly Section Line of said Section 19 a distance of 2639.63 Feet to a found US GLO 2 1/2" Brass Cap, This monument being disturbed and bent to the North, its position determined at the base of the monument, at the Northwest Section Corner of said Section 19.

Thence South 89°55'13" East along the Northerly Section Line of said Section 19 a distance of 2666.33 Feet to a found US GLO 2 1/2" Brass Cap at the Quarter Corner common to said Sections 18 and 19.

Thence North 00°38'49" West along the North-South MID-Section Line of said Section 18 a distance of 2642.84 Feet to a Found 1 ½" Aluminum Cap being the center Quarter Corner of said Section 18.

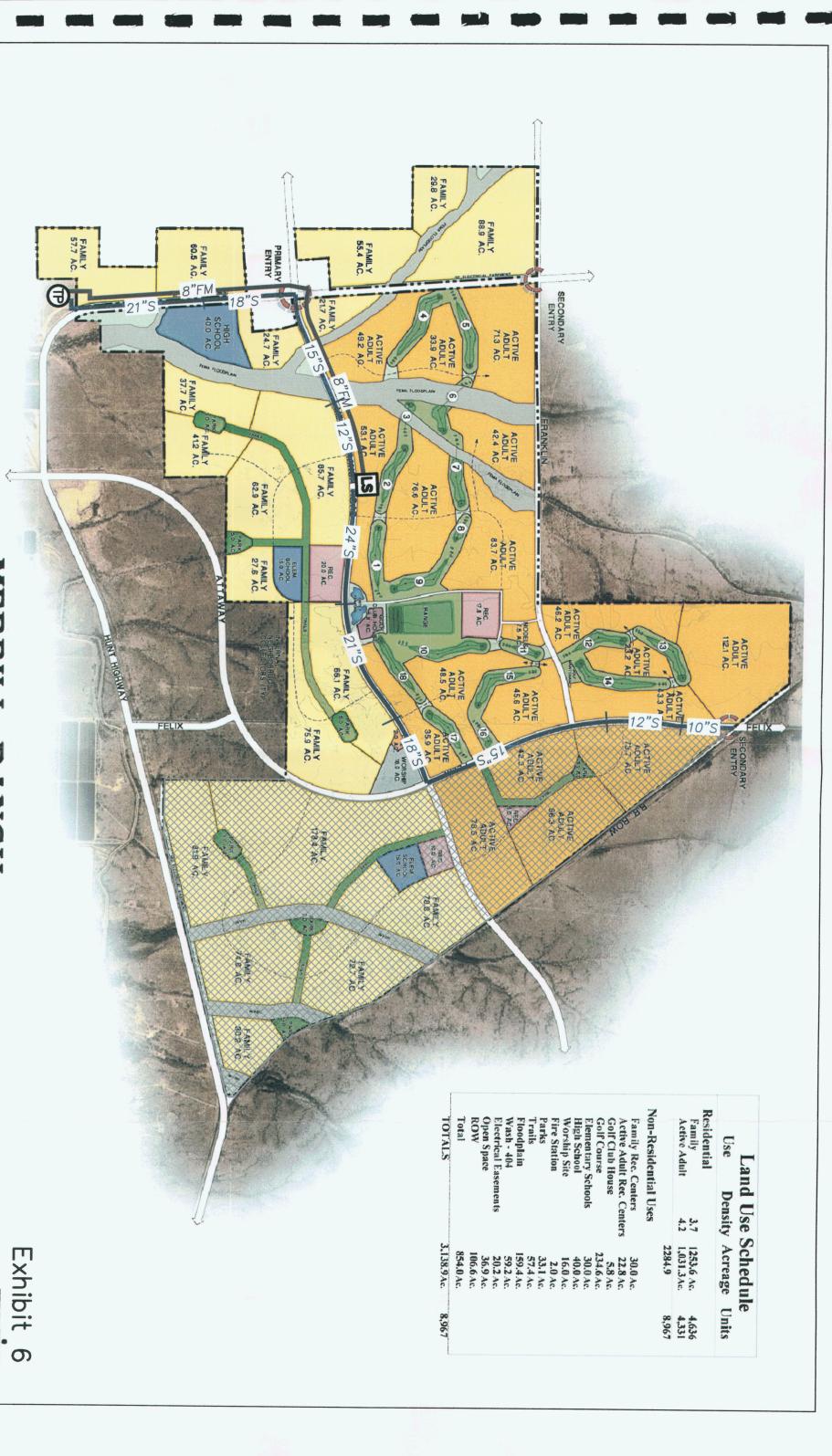
Thence North 00°38'34" West a distance of 2643.23 Feet to a found US GLO 2 1/2" Brass Cap at the North Quarter Corner of said Section 18, and the Point of Beginning for the herein described tract.

Said description contains 1,134.78 acres, more of less.

Y:\742MerrillRanch\04_Design\Survey\742 - Johnson Utilities 208 Expansion 8-30-04.doc

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Base mapping compiled from best available information.
All map data should be considered as preliminary, in need of ventilitation, and subject to change.
File: L 1,2428141 Concept with MPIRVI-Con E2, dwg

CONCEPTUAL MASTER PLAN E2

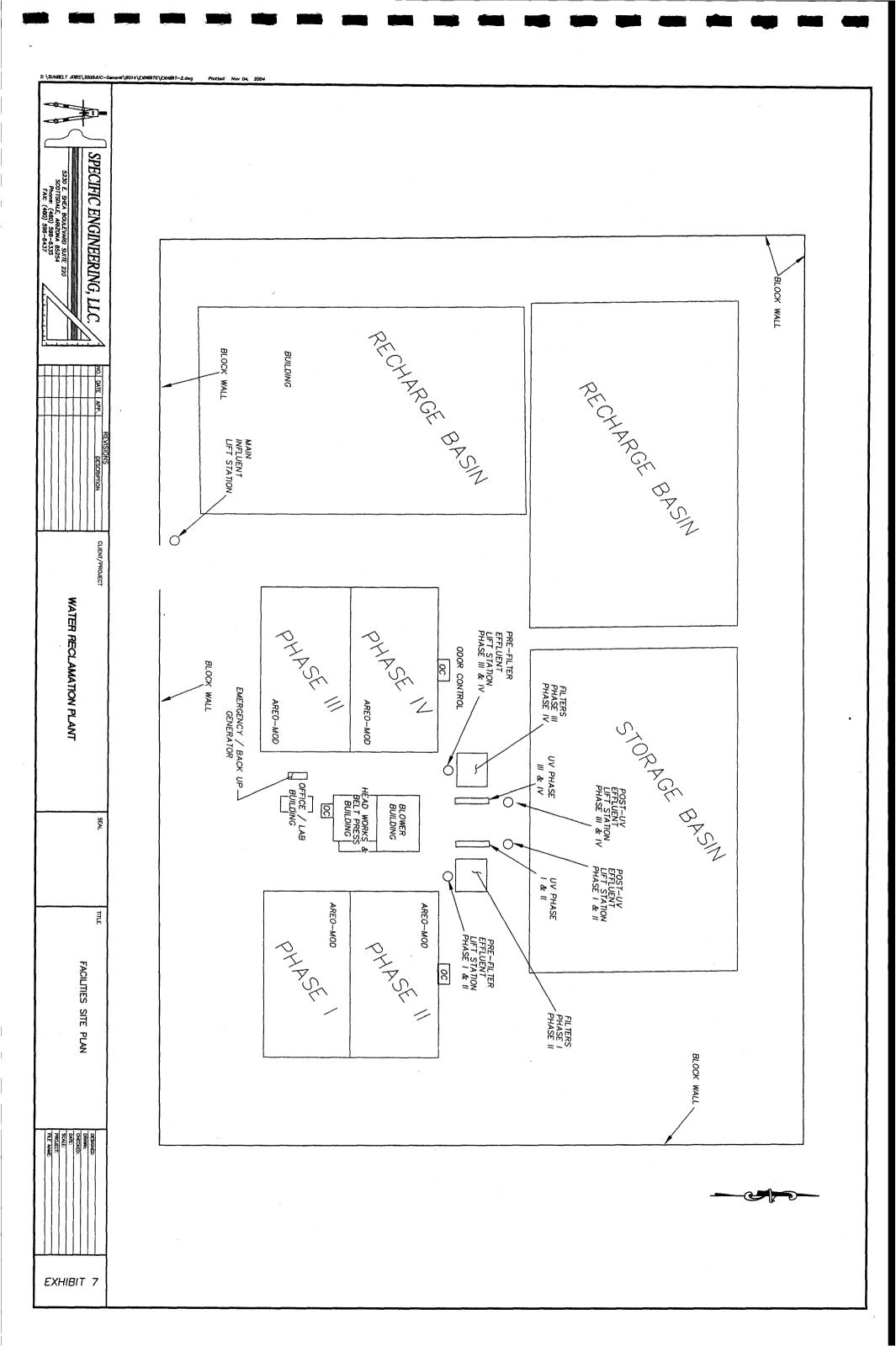
Florence,

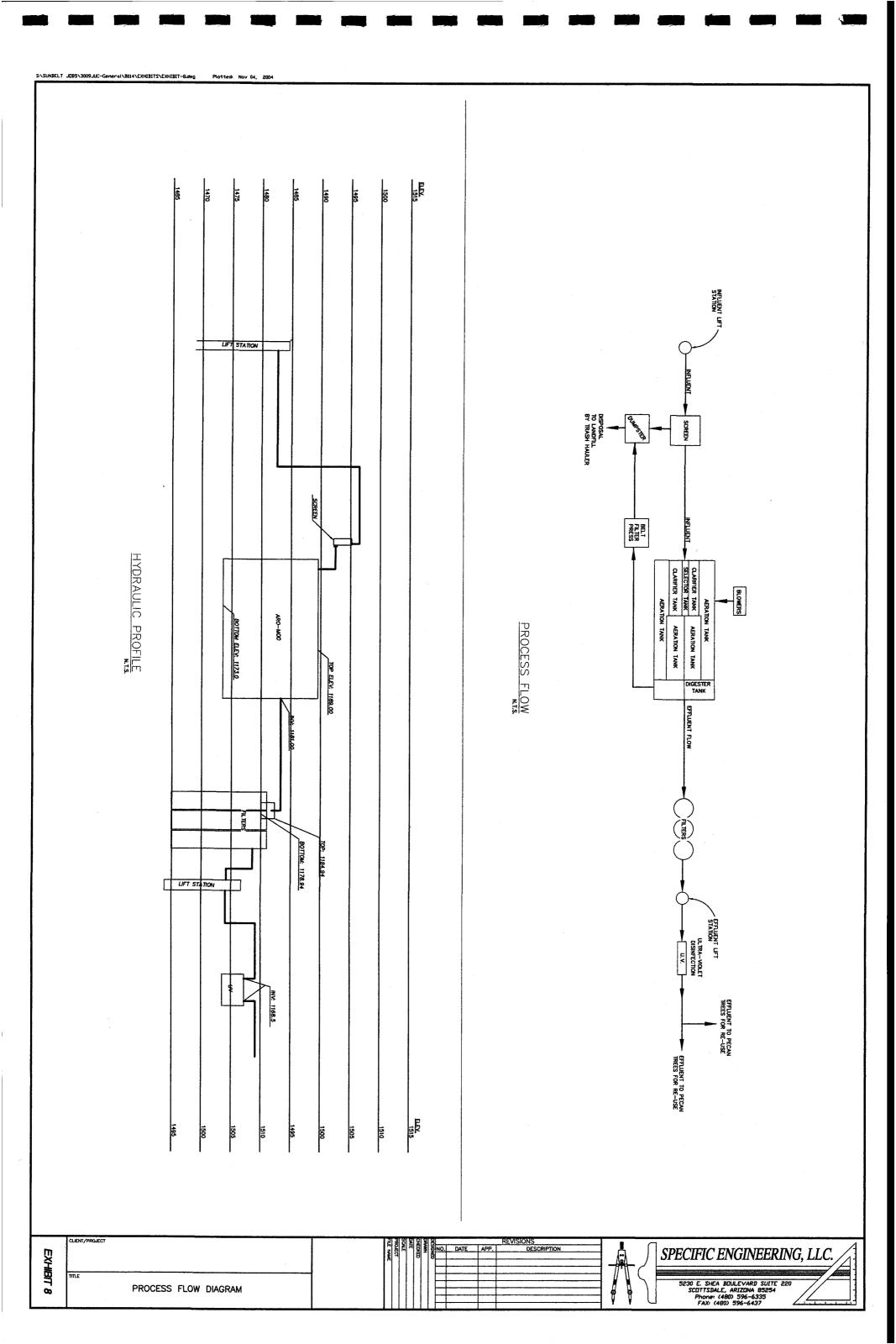
Arizona

The developer has reserved the right, without notice, to make changes to this map and other respects of the development to comply with governmental requirements and to fulfill its marketing objective.

800

SCALE : I' - 800 NORTH





DEMONSTRATION OF FINANCIAL CAPABILITY

The estimated costs for construction, operation, and closure of the facility are shown below:

	TABLE 9-1 L RANCH WATER RECLAMAT RUCTION, OPERATION, AND C	
Construction	Phase 1	\$6,827,493
	Phase 2	\$3,544,013
	Phase 3	\$5,575,200
	Phase 4	\$3,544,013
	Total	\$19,490,718
Operation		\$271,040
Closure		\$34,900

EXHIBIT 9A-1

TABLE 9						
MERRILL RANCH WATER RECLAMATION PLANT						
CONSTRUCTION COSTS						

CONSTRUCTION COSTS									
	Phase 1	Phase 2	Phase 3	Phase 4	Total				
Flow Design (MGD)	1.4	1.4	1.4	1.4	5.6				
Aero-Mod	\$1,080,000	\$1,080,000	\$1,080,000	\$1,080,000	\$4,320,000				
Installation Cost	\$300,000	\$225,000	\$250,000	\$225,000	\$1,000,000				
Concrete	\$905,000	\$870,000	\$870,000	\$870,000	\$3,515,000				
Sand Filter	\$160,000	\$160,000	\$160,000	\$160,000	\$640,000				
Concrete Basin	\$70,000	\$70,000	\$70,000	\$70,000	\$280,000				
Jones-Attwood Screen	\$130,000		\$130,000		\$260,000				
UV	\$350,000		\$350,000		\$700,000				
Concrete Basin	\$10,000		\$10,000		\$20,000				
Belt Press	\$150,000		\$150,000		\$300,000				
Odor Control	\$150,000		\$150,000		\$300,000				
Instrumentation	\$50,000		\$30,000		\$80,000				
Headworks Building	\$375,000		\$275,000		\$650,000				
Structural Engineer	\$10,000	\$5,000	\$10,000	\$5,000	\$30,000				
Mechanical Engineer	\$10,000				\$10,000				
Inside Finish	\$40,000		\$25,000		\$65,000				
Structural Coating	\$50,000	\$40,000	\$45,000	\$40,000	\$175,000				
Doors/Windows/Vents	\$20,000	\$10,000	\$10,000	\$10,000	\$50,000				
Lift Station/Pumps	\$150,000		\$225,000		\$375,000				
Steel Pipe	\$45,000	\$25,000	\$25,000	\$25,000	\$120,000				
PVC Pipe	\$35,000	\$35,000	\$35,000	\$35,000	\$140,000				
Excavate & Backfill	\$150,000	\$75,000	\$100,000	\$75,000	\$400,000				
Landscaping/Paving	\$200,000				\$200,000				
Fence	\$40,000				\$40,000				
Emergency Power	\$200,000				\$200,000				
HVAC -	\$25,000		\$10,000		\$35,000				
office/controllers Electrical 10%	\$468,000	\$250.500	\$400,000	\$259,500	¢1 207 000				
	\$468,000	\$259,500	\$400,000		\$1,387,000				
Contingincies (15%) APP Permit		\$227,250	\$438,000	\$227,250	\$1,506,450				
	\$150,000	#2 AP1 75A	64 040 000	\$2.001.750	\$150,000				
Subtotal CVI 9 D (1594)	\$5,936,950	\$3,081,750	\$4,848,000	\$3,081,750	\$16,948,450				
OH & P (15%)	\$890,543	\$462,263	\$727,200	\$462,263	\$2,542,268				
Total	\$6,827,493	\$3,544,013	\$5,575,200	\$3,544,013	\$19,490,718				
Cost/MG	\$4.88	\$2.53	\$3.98	\$2.53	\$3.48				

EXHIBIT 9A-2

ENGINEER'S OPINION OF PROBABLE COST PROJECT: MERRILL LIFT STATION & FORCE MAIN DATE: REVISED APRIL 07, 2004 SEWER FORCE MAIN

PROJECT NO. 3009

NO. of LOTS: 0

BY: Specific Engineering Services, LLC

Description	Unit	Approximate Quantity	Unit Price	TOTAL
10" C-900 DR18 PVC W/ FITTINGS	LF	25,300	14.00	\$354,200.00
8" DIP W/ FITTINGS	LF	80	35.00	\$2,800.00
4" DIP W/ FITTINGS	LF	40	20.00	\$800.00
4" CHECK VALVE	EA	1	860.00	\$860.00
4" GATE VALVE	EA	3	340.00	\$1,020.00
VALVE VAULT	EA	1	2,200.00	\$2,200.00
6" CLEANOUT	EA	26	600.00	\$15,600.00
CONTROL PANEL	EA	1	5,000.00	\$5,000.00
PUMP STATION (DUPLEX) COMPLETE	EA	1	75,000.00	\$75,000.00
COMB. AIR/VACUUM RELEASE VALVE & VAULT	EA	3	3,500.00	\$10,500.00
WARNING SIGNS	EA	15	150.00	\$2,250.00
DIRECT BURIAL	LF	80	120.00	\$9,600.00
4" WATER LINE WITH RISER	LF	40	20.00	\$800.00
6' CHAIN LINK FENCE/BLOCK WALL	LF	220	30.00	\$6,600.00
24' GATE(2-12' SWING GATES)	EA	1	1,000.00	\$1,000.00
ACCESS ROAD	SY	640	3.00	\$1,920.00
	TOTAL			\$490,150.00

EXHIBIT 9B

APPENDIX

л	Accidimed wastewater Re-Use I et mit Authorization
В	Aquifer Protection Permit Authorization
C	208 Amendment Checklist
D	ACC CC&N
E	Sewer Basin Flows
F	ADEO Correspondence

APPENDIX A
RECLAIMED WASTEWATER
RE-USE PERMIT AUTHORIZATION

RECLAIMED WASTEWATER
RE-USE PERMIT AUTHORIZATION

Authorization is Pending

APPENDIX B
AQUIFER PROTECTION PERMIT AUTHORIZATION

AQUIFER PROTECTION PERMIT AUTHORIZATION

APP Authorization is Pending

APPENDIX C
208 AMENDMENT CHECKLIST

MERRILL RANCH PHASE 1 AMENDMENT 208 AMENDMENT CHECKLIST SECTION 208, CLEAN WATER ACT

AUTHORITY

1. Requirement: - Proposed Designated

Proposed Designated Management Agency (DMA) shall self-certify that it has the authorities required by Section 208(c)(2) of the Clean Water Act to implement the plan for its proposed planning and service areas. Self-certification shall be in the form of a legal

opinion by the DMA or entity attorney.

Summary: Does not apply; Johnson Utility Company is not a DMA.

Addressed on Page: 5.

20-YEAR NEEDS

2. Requirement:: - Clearly describe the existing wastewater (WW) treatment facilities:

- Describe the existing WWTP facilities.

Summary: Currently, there are no existing facilities in the vicinity of the Merrill

Ranch Phase 1 area. A WWTP is proposed for each site. All plants will be Aero-mod Extended aeration treatment plants. The Merrill Ranch Phase 'development will have a total capacity of 2.5 MGD.

Addressed on Page: 1.

3. Requirement:: - Show WWTP certified and service areas for private utilities and

sanitary district boundaries if appropriate.

Summary: Johnson Utilities Company has been formed as a utility company

registered with the Arizona Corporation Commission to provide water and sewer service for the Johnson Ranch area. The current Franchise Areas are as shown in Exhibit 2. The existing CC&N

boundaries are as shown on Exhibit 3.

Addressed on Page: 5.

4. Requirement:: Clearly describe alternatives and the recommended WWTP plan:

- Provide POPTAC population estimates (or COG-approved estimates only where POPTAC not available) over 20-year period.

Summary: The total planning area for Merrill Ranch Phase 1 area totals 2110

acres with 7997 dwelling units. The project will be developed in approximately four phases consisting primarily of family and adult

residential property.

Addressed on Page: 9,10, and Appendix E.

5. Requirement:: - Provide wastewater flow estimates over the 20-year planning

period.

Summary: Wastewater flow estimates are: 2.6 per/D.U. x 90 GPCD = 234

Gal/D.U.

Treatment facility estimates are: Merrill Ranch, Phase 1, 2.5 MGD.

It is anticipated that the wastewater treatment facilities will be at full

capacity within the next 15 to 20 years.

Addressed on Page: 9,10, and Appendix E.

6. Requirement:: - Illustrate the WWT planning and service areas.

Summary: The WRP will service Merrill Ranch project within the CC&N areas.

Addressed on Page: 7, 8, and Exhibits 5a - 5d, and 6.

7. Requirement:: - Describe the type and capacity of the recommended WRP Plant.

Summary: The WRP will be sized for a total capacity of 2.5 MGD. The plant

will be Aero-Mod Extended Aeration Water Reclamation Plant with

effluent reuse on turf areas.

<u>Addressed on Page:</u> 2, 4, 6, 8, and 12...

- Identify water quality problems, consider alternative control measures, and recommend solution for implementation.

Summary:

Johnson Utilities service area. Johnson Utilities will work improve the quality of the groundwater in this area by meeting effluent reuse standards for open-access golf courses and meeting Class preclaimed water requirements, which is equivalent to secondary treatment and disinfection. To prevent future nitrate problems, Johnson Utilities will not approve septic tanks, except for existing or previously approved septic tank systems for developments within the the Johnson Utilities service area.

Addressed on Page:

2, 3, 38, and 12.

9. Requirement:-

If private WWTP utilities with certificated areas are within the proposed regional service area, define who (municipal or private utility) serves what area and when. Identify whose sewer lines can be approved in what areas and when?

Summary:

A portion of Merrill Ranch project is located within the existing sewer and water certificated areas of Johnson Utilities, L.L.C.

Addressed on Page;

Exhibits 2 and 3.

10. Requirement::

- Describe method of effluent disposal and reuse sites (if appropriate).

Summary:

The treated effluent will be used for irrigation of the golf courses that have been constructed within the projects as well as irrigation uses within other open spaces and landscaping within the developments.

Addressed on Page:

2, 8, and 9.

11. Requirement::

- If Sanitary Districts are within a proposed planning or service area, describe who serves the Sanitary Districts and when.

Summary:

There are no existing Sanitary Districts in the proximity of the Merrill Ranch project, other than Johnson Utilities, L.L.C.

Addressed on Page:

1.

- Describe the ownership of land proposed for plant sites and reuse

areas.

Summary:

The proposed sites for the wastewater treatment plants are owned by

various entities. The reuse areas (golf course, open space, etc.) is currently owned by the corresponding entity. George H. Johnson, is

the owner of Johnson Utilities Co., L.L.C.

Addressed on Page:

3, and 7.

13. Requirement::

- Address time frames in the development of the treatment works.

Summary:

The first phase, phase A, of the WRPs will initially commence

operation in mid 2005. the project is expected to be completed

within the next 5 years.

Addressed on Page:

14. Requirement::

- Address financial constraints in the development of the treatment

works.

Summary:

The project financing for Johnson Utilities is described within

Section 8, Project Financing.

Addressed on Page:

17 and Exhibit 9.

15. Requirement::

- Describe how discharges will comply with EPA municipal and

industrial stormwater discharge regulations (Section 405, CWA).

Summary:

All runoff will be directed through landscaped retention basins along

with sediment removal and bio-filtration.

Addressed on Page:

4, 7, 34, and 12.

16. Requirement::

- Describe how open areas and recreational opportunities will result

from improved water quality and how those will be used.

Summary:

Effluent treated to the required standards will be used to irrigate the

golf course, neighborhood parks, trails and other open activity areas, thus encouraging recreational opportunities for the area residents.

Addressed on Page: 5, 7, 8, 9, and 12.

- Describe potential use of lands associated with treatment works and

increased access to water-based recreation, if applicable.

Summary:

The property contained within the required setbacks will be used for acceptable non-residential uses such as Golf Course corridors which will provide beneficial activities and services to the area residents. Additional uses will include equestrian facilities, RV storage and

open activity areas.

Addressed on Page:

1, 2, 4, 5, 7, and 12.

REGULATIONS

18. Requirement::

- Describe types of permits needed, including NPDES, APP and

reuse.

Summary:

Permits required for the project include an Individual Aquifer Protection Program Permit (APP), and a Reclaimed Water Permit. The APP and Reclaimed Permit will be applied for starting in 2001. A National Pollution Discharge Elimination System Permit for effluent discharge and sludge disposal will be required for the Merrill Ranch only. The permit will be applied for as part of the phasing plan for the WWTP. A Stormwater Pollution Permit will be applied for as part of the grading permit application.

Addressed on Page:

Section 4

19. Requirement::

- Describe restrictions on NPDES permits, if needed, for discharge

and sludge disposal.

Summary:

A NPDES Permit for discharge will be required for the Merrill Ranch

WRP.

Addressed on Page:

14

- Provide documentation of communication with ADEQ Permitting Section 30 to 60 days prior to public hearing regarding the need for specific permits.

Summary:

Meetings have been held with representatives from the ADEQ Permitting Section, and representatives of CAAG throughout the development of this plan. Specific Engineering, LLC has been in regular contact with ADEQ engineering department, and any ADEQ meeting will be attended by Specific Engineering, LLC staff to discuss modifications to the APP permit.

Addressed on Page:

Appendix F

21. Requirement::

- Describe pre-treatment requirements and method of adherence to requirements (Section 208 (b)(2)(D), CWA).

Summary:

A pre-treatment program has been proposed in conformance with the Clean Water Act for Non-Domestic Waste.

Addressed on Page: 14.

22. Requirement::

- Identify, if appropriate, specific pollutants that will be produced from excavations and procedures that will protect ground and surface water quality (Section 208 (b)(2)(K) and Section 304, CWA).

Summary:

A NPDES Stormwater Pollution Prevention Permit will be obtained by the contractor prior to all construction of facilities within the proposed construction sites.

Addressed on Page:

23. Requirement::

- Describe alternatives and recommendation in the disposition of sludge generated. (Section 405 CWA)

Summary:

Sludge will be disposed of at a landfill which is state certified to accept wastewater sludge. Butterfield Station, located in Mobile, Arizona, will accept sludge from the wastewater treatment plant for disposal.

Addressed on Page:

14 and 15.

14.

- Define any non-point issues related to the proposed facility and

outline procedures to control them.

Summary:

The only opportunity for non-point discharges is from the golf courses. The courses have been designed to retain runoff within the

fairways and corridors.

Addressed on Page:

ge: 15.

25. Requirement::

- Define the process to handle all mining runoff, orphan sites and

underground pollutants, if applicable.

Summary:

Not applicable. There are no mining activities involved within this

project.

Addressed on Page:

N/A.

26. Requirement::

- If mining related, define where collection of pollutants has

occurred, and what procedures are going to be initiated to contain

contaminated areas.

Summary:

Not applicable. There are no mining activities involved within this

project.

Addressed on Page:

N/A.

27. Requirement::

- If mining related, define what specialized procedures will be

initiated for orphan sites, if applicable.

Summary:

Not applicable. There are no mining activities involved within this

project.

Addressed on Page:

N/A.

CONSTRUCTION

28. Requirement::

- Define construction priorities and time schedules for initiation and

completion.

Summary:

The WRP will be built starting in 2005, and should be competed by

2006.

Addressed on Page:

5, 6, and 12.

29. Requirement::

- Identify agencies who will construct, operate and maintain the

facilities and otherwise carry out the plan.

Summary:

Johnson Utilities will provide water and sewer service for the

Johnson Ranch Project. Johnson Utilities will construct, operate and

maintain the water and sewer facilities.

Addressed on Page:

1.

30. Requirement::

- Identify construction activity-related sources of pollution and set

forth procedures and methods to control, to the extent feasible, such

sources.

Summary:

The contractor shall comply with NPDES and OSHA Permit

regulations as they apply to construction activities and materials.

Addressed on Page:

14 and 15.

FINANCING AND OTHER MEASURES NECESSARY TO CARRY OUT THE PLAN

31. Requirement::

- If plan proposes to take over certificated private utility, describe

how, when and financing will be managed.

Summary:

This item is not applicable. Johnson Utilities is the utility company

approved by ACC.

Addressed on Page:

17.

- Describe any significant measure necessary to carry out the plan,

e.g., institutional, financial, economic, etc.

Summary:

The project financing for Johnson Utilities is described within

Section 8, Project Financing. The CC&N has been approved by the

ACC.

Addressed on Page:

17 and Exhibit 9.

33. Requirement::

- Describe proposed method(s) of community financing.

Summary:

The project financing for Johnson Utilities is described within

Section 8, Project Financing.

Addressed on Page:

17, and Exhibit 9.

34. Requirement::

- Provide financial information to assure DMA has financial

capability to operate and maintain wastewater system over its useful

life.

Summary:

Although Johnson Utilities is not a DMA, the project financing for

Johnson Utilities is described within Section 7, Project Financing.

Addressed on Page:

17.

35. Requirement::

- Provide a time line outlining period of time necessary for carrying

out plan implementation.

Summary:

The Builders have estimated 5 years for the project to be built out.

At full buildout, the wastewater treatment plant will have a capacity of 2.5 MGD (Merrill Ranch), to serve the needs of the project. Treatment and collection capacity will be built in phases to match the growth of the development. It is anticipated that the plant will be

operating at 100% efficiency within the next 15 to 20 years.

Addressed on Page:

6, and Appendix E.

-Provide financial information indicating the method and measures

necessary to achieve project financing. (Section 201 CWA or

Section 604 may apply.)

Summary:

The project financing for Johnson Utilities is described within

Section 8, Project Financing.

Addressed on Page:

17, and Exhibit E.

IMPLEMENTABILITY

37. Requirement::

Describe impacts and implementability of Plan:

- Describe impacts on existing wastewater (WW) facilities, e.g.,

sanitary district, infrastructure/facilities and certificated areas.

Summary:

There are no sanitary districts within the area, and the existing wastewater treatment facilities are owned and operated by Johnson Utilities Co., L.L.C. Johnson Utilities is currently serving a portion of the certificated area, and the development of the WRP will allow

for expansion of its treatment capabilities.

Addressed on Page:

3, 5, 7, 11, and 12 and Exhibits 2 and 3.

38. Requirement: - Describe how and when existing package plants will be connected to a

regional system.

Summary:

There are no existing regional wastewater treatment plants within

the area of Merrill Ranch, and the system will therefore not be

connected to one.

Addressed on Page:

1, 3, 4, and 7.

39. Requirement: - Describe the impact on communities and businesses affected by the plan.

Summary:

The proposed water reclamation plant will have a beneficial affect on the area by providing better treatment of wastewater, eliminating a potential source of groundwater contamination, creating capacity for growth by providing the necessary infrastructure and creating recreational areas by the reuse of treated effluent as an irrigation source. The facilities also make housing available for the work force in the Florence area and creates employment opportunities in the southeast valley area.

Addressed on Page:

7 and 8.

40. Requirement::

- If a municipal wastewater (WWT) system is proposed, describe how WWT service will be provided until the municipal system is completed; i.e., will package plants and septic systems be allowed and under what circumstances. (Interim services.)

Summary:

Sewer service will be provided by an Aero-Mode Extended Aeration mechanical treatment facility will be operational before the proposed subdivisions are developed. It is anticipated the mechanical treatment plant will be operational by 2005.

Addressed on Page:

3, 5, and 6.

PUBLIC PARTICIPATION

41. Requirement::

- Submit copy of mailing list used to notify the public of the public hearing on the 208 amendment. (40 CFR, Chapter 1, Part 25.5)

Summary:

Provided by CAAG.

Addressed on Page:

N/A.

42. Requirement: List location where documents are available for review at least 30 days before public hearing.

Summary:

Provided by CAAG.

Addressed on Page:

N/A.

43. Requirement:: - Submit copy of the public notice of the public hearing as well as an

official affidavit of publication from the area newspaper. Clearly show the announcement appeared in the newspaper at least 45 days

before the hearing.

Summary:

Provided by CAAG.

Addressed on Page:

N/A.

44. Requirement::

- Submit affidavit of publication for official newspaper publication.

Summary:

Provided by CAAG.

Addressed on Page:

N/A.

45. Requirement::

- Submit responsiveness summary for public hearing.

Summary:

Provided by CAAG.

Addressed on Page:

N/A.

APPENDIX D ACC CC&N

ACC CC&N

CC & N is Pending

APPENDIX E SEWER BASIN FLOWS

							S PHASE			
Subbasin	Zoning	Area	Common/		Population		Storm	Avg. Daily	Peak Dry	Peak W
Area		Sewered	School	Units		Peaking	Inflow	Flow	Weather	Weath
		(Acres)	Area	Sewered		Factor	(MGD)	(MGD)	Flow	Flow
			Sewered (Acres)						(MGD)	(MGD
A-AA-4.2	R-2	112.1		471	1224	2.34	0.028	0.110	0.258	0.2
B-AA-4.2	R-2	43.3		182	473	2.67	0.011	0.043	0.114	0.1
C-AA-4.2	R-2	23.2		97	253	3.02	0.006	0.023	0.069	0.0
D-AA-4.2	R-2	46.2		194	505	2.64	0.012	0.045	0.120	0.1
E-AA-4.2	R-2	45.6		192	498	2.65	0.011	0.045	0.119	0.
F-AA-4.2	R-2	7.5		32	82	3.62	0.002	0.007	0.027	0.0
G-AA-4.2	R-2	48.5		204	530	2.62	0.012	0.048	0.125	0.
H-AA-4.2	R-2	35.9		151	392	2.76	0.009	0.035	0.097	0.1
-COMM	C-2	0	6.8			3	0.002	0.007	0.020	0.0
J-CHC	C-2	0	16			3	0.004	0.016	0.048	0.0
K-F-3.7	R-1	66.1		245	636	2.55	0.017	0.057	0.146	0.1
	R-1	75.9		281	730	2.85	0.019	0.066	0.187	0.2
M-ESCL	C-2		15			3	0.004	0.015	0.045	0.0
	R-1	27.6		102	266	3.02	0.007	0.024	0.072	0.0
O-AA-4.2	R-2	53.1		223	580	2.58	0.013	0.052	0.135	0.
P-AA-4.2	R-2	76.6		322	836	2.45	0.019	0.075	0.184	0.2
Q-AA-4.2	R-2	83.7		352	914	2.42	0.021	0.082	0.199	0.2
R-AA-4.2	R-2	42.4		178	463	2.69	0.011	0.042	0.112	0.1
S-REC	C-2		17.8			3	0.004	0.018	0.053	0.0
T-REC	C-2		20			3	0.005	0.020	0.060	0.0
	R-1	85.7		317	824	2.45	0.021	0.074	0.182	0.2
	R-1	62.9		233	605	2.57	0.016	0.054	0.140	0.1
	R-1	41.2		152	396	2.76	0.010	0.036	0.098	0.1
	R-1	37.7		139	363	2.82	0.009	0.033	0.092	0.1
	R-1	24.7		91	238	3.08	0.006	0.021	0.066	0.0
	R-2	49.2		169	439	2.72	0.012	0.040	0.108	0.1
AA-AA4.2		33.9		91	237	3.06	0.008	0.021	0.065	0.0
BB-AA4.2		71.3		189	491	2.65	0.018	0.044	0.117	0.
	R-1	88.9		329	855	2.44	0.022	0.077	0.188	0.2
	R-1	29.8		110	287	2.93	0.007	0.026	0.076	0.0
	R-1	55.4		205	533	2.62	0.014	0.048	0.126	0.1
	R-1	21.7		80	209	3.15	0.005	0.019	0.059	0.0
	R-1	60.5		224	582	2.58	0.015	0.052	0.135	0.
	R-1	57.7		213	555	2.6	0.014	0.050	0.130	0.1
	C-2		40			3	0.010		0.120	0.
FIRE STA			2			3	0.001	0.002	0.006	0.0
PARK	OP DAG	15	2			3	0.001	0.002	0.006	0.0
GLFCRS	RST RMS	234.6	5			3	0.001	0.005	0.015	0.0
TOTAL		1757.9	124.6	5767.5	14995.4		0.4	1.5	3.9	
	arcels withi					a portion of				
	R-1	100		370			0.025	0.087	0.208	0.2
	R-1	330		1221	3175		0.083	0.286	0.597	0.6
	R-1	40		148	385	2.77	0.010	0.035	0.096	0.
	R-1	172.5		638	1659	2.25	0.043	0.149	0.336	0.3
TOTAL		642.5	0	2377.3	6180.9	9.5	0.2	0.6	1.2	
TOTAL		2150.8					0.6		5.2	

APPENDIX F
ADEQ CORRESPONDENCE

ADEQ CORRESPONDENCE

Correspondence to be inserted by CAAG

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ATTACHMENT 2

FLORENCE, ARIZONA

MASTER WASTEWATER COLLECTION SYSTEM REPORT PULTE DEVELOPMENT WEST OF FELIX ROAD

NOVEMBER 2004

Prepared For: Pulte Homes 15333 N. Pima Road, Suite 300 Scottsdale, Arizona 85260

Prepared By: Jack Johnson Company 5745 N. Scottsdale Road, Suite 130 Scottsdale, Arizona 85250



FLORENCE, ARIZONA

MASTER WASTEWATER COLLECTION SYSTEM REPORT PULTE DEVELOPMENT WEST OF FELIX ROAD

NOVEMBER 2004



PROJECT ENGINEER

JACK JOHNSON COMPANY 5745 N. SCOTTSDALE ROAD, SUITE 130 SCOTTSDALE, ARIZONA 85250

> Telephone: (480) 214-0370 Facsimile: (480) 214-0356

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Introduction

Project Location

The Pulte Development portion of Merrill Ranch West of Felix Road (the Project) lies within the jurisdiction of the Town of Florence. The Project is a 2,000-acre (±) mixed-use Planned Unit Development (PUD) with low to medium-high density neighborhood housing, with several areas reserved for neighborhood businesses and commercial uses. An extensive trail network connects the lineal park system and natural desert spaces and community parks and is a part of the Open Space System. The Project is located primarily on desert scrublands, crossed by various minor drainage courses. There is a designated Federal Emergency Management Agency (FEMA) Flood Zone "A" on the western edge of the Merrill Ranch. Hunt Highway runs through the property.

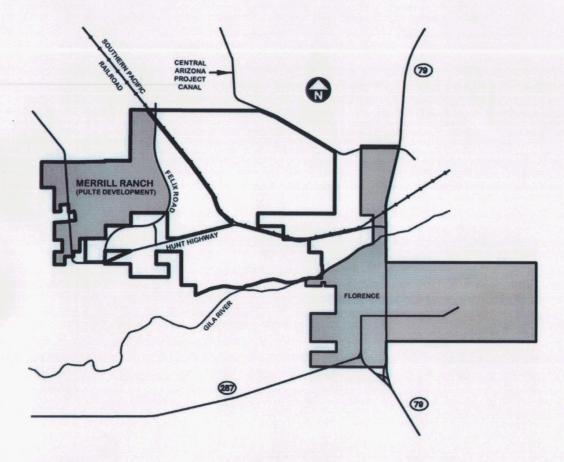


Figure 1. Project Location Map

Scope

The scope of this report is to provide the Master Wastewater Collection System design for the Project.

Specifically this report includes the following for the Project:

- Jurisdictional design criteria
- Wastewater system loads
- Hydraulic model for trunklines

Specifically this report does not address the following:

- Individual community wastewater main lengths, sizes, and locations (although approximate interceptor & trunk line point loading locations for developments/properties/parcels are indicated).
- □ Site specific or detailed design of infrastructure.



Jurisdictional Design Criteria

Jurisdiction

The Project lies within the jurisdictions of:

- Johnson Utilities Company
- □ Town of Florence, Arizona
- State of Arizona

Design Source Documents

The minimum design criteria, against which the Project and all associated developments are measured, as pertaining to wastewater systems, shall be in accordance with the following documents:

- Johnson Utilities Company: Johnson Utilities Company Design Guide and Standard Details, May 2003.
- □ Town of Florence: Development Codes Zoning Ordinance Subdivision Regulations, June 2000
- Arizona State: Engineering Bulletin No. 11 "Minimum Requirements for Design, Submission of Plans and Specifications of Sewage Works" Arizona Department of Environmental Quality, July 1978.
- Arizona State: Arizona Administrative Code R18-9-E301D

If, in any instance documents conflict, the most restrictive rule or regulation shall apply from the standpoint of capacity, level of service and public safety. The Engineer of Record shall bear the responsibility of interpretation of all such conflicts.

Wastewater System Loads

Loading Calculations

Wastewater loads were calculated using the methods prescribed by Johnson Utilities Company and were based on available planning and/or density estimations at the time of this report. Peaking factors have been applied per parcel or portions of parcels as defined by trunkline load points. Appropriate peaking factors shall be applied to each associated interior project/parcel for the purpose of designing local wastewater mains.

See "Wastewater Loads" (Appendix 1)

	Exit Flows
1.7 MGD	Treatment (Ave Day + Infiltration)
4.4 MGD	Collection (Peak Day + Infiltration)
3,058 GPM	Collection (Peak Day + Infiltration)

Table 1. Exit Flows



Hydraulic Model Parameters

Design Parameters & Assumptions

- □ Loads/Flows (as outlined in "Wastewater Loads")
- Pipes
 - Manning's "n" roughness coefficient = 0.013
 - Minimum design slopes:

	esign Slopes
	Pipes (ADEQ)
(velocities ≥ 2.0	0 fps & n=0.013)
Diameter (in)	Slope (ft/ft)
8	0.0033
10	0.0024
12	0.0019
15	0.0014
18	0.0011
24	0.00077

Table 2. Minimum Design Slopes

- Manholes
 - Headloss Standard Method

Hydraulic Model

Modeling Methodology

The software design package selected for electronic modeling is Haestad Methods SewerCad v5.5.

The output data provided/calculated by the electronic model is:

- □ System Schematic
- Manhole Report (rim elevation, sump elevation, headloss coefficient, base flow, total flow, velocity, HGL in, HGL out, EGL in, EGL out)
- Gravity Pipe Report (length, section size, Manning's n, constructed slope, depth in, depth out, total flow, design capacity, excess design capacity)
- Outlet Report (rim elevation, sump elevation, total flow, HGL in, HGL out, EGL in, EGL out)

See "Hydraulic Model Output Data" (Appendix 2)

Development & Infrastructure Phasing & Schedule Estimates

Phasing of the wastewater collection system infrastructure will follow and be dependent upon the sequence of project approvals. For any given sub-division all necessary downstream trunklines shall be constructed and approved prior to any sub-division being allowed to make a connection.

Conclusions

The data supplied by the model demonstrates that the system design represents an adequately sized system under gravity conditions for the assumptions as listed herein.

MERRILL RANCH - PULTE DEVELOPMENT WEST OF FELIX ROAD WASTEWATER LOADS 10/20/2004

Post Day 1. Mat Day					Resid	Residential				Comn	Commercial			Infiltration		Design	Design Flows (Maximum)	(E)
Mil. D. U. Flow Pop. Paskring Flow Graph Graph	,			Ave. Day		Pea	ık Day		Avera	ge Day	Peak	Day	(no design	peaking facto	rs applied)	Treatment	Collection	-co
(4) (4) <th>Parcel</th> <th>¥</th> <th>o O</th> <th>Flow</th> <th>Pop</th> <th>Peaking</th> <th>Flo</th> <th>\</th> <th>Area</th> <th>Flow</th> <th>Flo</th> <th>M.</th> <th>Area</th> <th>Flo</th> <th>M</th> <th>Flow</th> <th>Flow (System Loading)</th> <th>oading)</th>	Parcel	¥	o O	Flow	Pop	Peaking	Flo	\	Area	Flow	Flo	M.	Area	Flo	M	Flow	Flow (System Loading)	oading)
117 86 13850 146 280 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 6500 35 1720 1720 35 35 35 36 0 0 0 0 0 27 6500 35 4500 10 0			(±)	(pdb)	(bers.)	Factor	(pd6)	(mdg)	(acre)	(pdb)	(pd6)	(mdB)	(acre)	(pdb)	(mdB)	(pdb)	(pdf)	(mdg)
92 137 22,039 356 29,0 65,2374 465 0 0 0 0 0 0 27 6,066 1 28 1 702 1 72,234 1 96 22,274 42 0 0 0 0 27 6,066 1 19 1 10 1 30,06 2 12 3 14 7,5113 42 0 0 0 0 0 27 6,066 1 19 1 11 1 30,06 2 12 3 14 2 14,267 6 0	-	117	98	13,950	155	3.62	50,500	35	0	0	0	0	22	5,520	4	19,470	56,020	39
128 106 17204 191 362 622710 43 0 0 0 0 27 6,088 118 118 1190 234 262 314 6273 42 0 0 0 0 24 6,088 118 118 1190 12300 286 234 6273 42 0 0 0 0 24 6,088 130 144 125 28248 236 628 60 0	2	92	137	32,039	356	2.90	92,914	65	0	0	0	0	33	8,150	9	40,189	101,064	70
189 102 23821 268 3.14 75,113 62 0	3	128	106	17,204	191	3.62	62,278	43	0	0	0	0	27	6,808	S.	24,011	980'69	48
118 118 130 column 212 3.14 59,773 42 0 <td>4</td> <td>93</td> <td>102</td> <td>23,921</td> <td>266</td> <td>3.14</td> <td>75,113</td> <td>52</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>24</td> <td>6,085</td> <td>4</td> <td>30,006</td> <td>81,198</td> <td>56</td>	4	93	102	23,921	266	3.14	75,113	52	0	0	0	0	24	6,085	4	30,006	81,198	56
91 441 33,101 388 2.90 65,992 67 0 0 0 19 44,423 90 175 29,248 2.26 43,887 30 0 0 0 0 0 19 4,440 90 175 29,248 3.25 2.30 64,887 30 0 0 0 0 0 0 19 44,425 143 140 2.744 12,148 55,44 12,148 65 0	2	118	118	19,036	212	3.14	59,773	42	0	0	0	0	8	7,533	2	26,569	67,306	47
130 75 12,18 326 3,887 30 0 0 0 0 14,405 119 1175 18,341 216 24,887 30 0 0 0 0 14,405 119 1175 18,341 210 314 12,1718 86 0 0 0 0 30 1740 113 88 14,247 344 274 12,1718 86 0 0 0 0 23 2,440 113 88 14,247 45,427 41,1718 86 0 0 0 0 23 7,440 143 88 110 0<	9	91	141	33,101	368	2.90	95,992	29	0	0	0	0	क्ष	8,420	9	41,521	104,412	73
90 125 28,284 2.50 48,820 45 0 0 0 0 0 7,495 149 177 18941 2.74 21,718 45,820 0 0 0 0 0 0 0 4465 11,300 143 189 14,423 454 2.74 121,718 66 0 0 0 0 0 0 455 11,300 143 189 14,423 454 2.74 121,718 66 0 <td>7</td> <td>130</td> <td>75</td> <td>12,118</td> <td>135</td> <td>3.62</td> <td>43,867</td> <td>S</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>19</td> <td>4,795</td> <td>3</td> <td>16,913</td> <td>48,662</td> <td>용</td>	7	130	75	12,118	135	3.62	43,867	S	0	0	0	0	19	4,795	3	16,913	48,662	용
119 117 18,91 44,223 494 23,44 68,476 61,00 0 0 0 0 0 0 0 0 0 0 0 0 1,1300 113 189 14,247 159 32,4 15,174 36 0 0 0 0 0 45 1,1300 1137,121 142 22,834 25,6 31,4 72,014 50 0	8	8	125	29,248	325	2.90	84,820	29	0	0	0	0	೫	7,440	2	36,688	92,260	25
94 190 44,423 484 274 177,18 86 0 0 0 46 71,00 76 119 27,961 150 61,074 86 0 0 0 0 23 51,83 176 119 27,961 151 2.90 81,086 6 0 0 0 0 23 51,13 32 63 11,025 114 3.62 41,981 20 0 0 0 0 0 28 51,13 32 63 11,025 114 3.62 41,981 20 0	6	119	117	18,941	210	3.14	59,476	4	0	0	0	٥	æ	7,495	2	26,436	66,971	47
113 88 14,247 158 3.62 51,514 36 0 0 0 28 5,638 137,121 142 27,994 236 3.14 72,014 50 0 0 0 28 5,138 16 116 22,934 256 3.14 72,014 50 0 0 0 0 28 5,178 16 50 11,587 129 36 3,148 12,014 0	10	8	190	44,423	494	2.74	121,718	82	0	0	0	0	45	11,300	8	55,723	133,018	92
76 119 27.5461 311 2.90 81.086 56 0 0 0 28 7/13 16 50 11.597 129 3.62 41.9814 29 0 0 0 0 28 7/13 32 6 50 11.597 129 3.62 41.9814 29 0 0 0 0 28 7/13 32 6 10.23 114 3.62 3.705 1 0 0 0 0 0 0 12 2.960 103 10.664 186 3.62 3.705 0 <th< td=""><td>11</td><td>113</td><td>88</td><td>14,247</td><td>158</td><td>3.62</td><td>51,574</td><td>98</td><td>0</td><td>0</td><td>0</td><td>0</td><td>23</td><td>5,638</td><td>4</td><td>19,885</td><td>57,212</td><td>40</td></th<>	11	113	88	14,247	158	3.62	51,574	98	0	0	0	0	23	5,638	4	19,885	57,212	40
137,121 142 22,934 255 3,14 72,014 50 0 0 0 36 9,075 16 41,987 129 362 3,14 72,014 50 0 0 0 0 36 9,075 32 63 10,236 114 3,62 3,7051 26 0 0 0 0 16 4,050 75 119 27,813 309 2,90 80,688 56 0 0 0 0 0 16 4,050 142 82 19,263 2,14 3,14 60,288 56 0 </td <td>12</td> <td>92</td> <td></td> <td>27,961</td> <td>311</td> <td>2.90</td> <td>81,086</td> <td>26</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>78</td> <td>7,113</td> <td>2</td> <td>35,073</td> <td>88,198</td> <td>61</td>	12	92		27,961	311	2.90	81,086	26	0	0	0	0	78	7,113	2	35,073	88,198	61
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32 63 10,255 114 362 37,051 26 0 0 0 0 16 4,050 103 1139 27,813 310 2.90 2.90 60,688 56 0 0 0 0 2.6 6,580 103 113 16,644 185 3.62 60,288 42 0 0 0 0 2.0 2.6 6,580 142 82 18,253 214 3.64 23,707 3.0 0 <td>14</td> <td>16</td> <td></td> <td>11,597</td> <td>129</td> <td>3.62</td> <td>41,981</td> <td>53</td> <td>0</td> <td>0</td> <td>0</td> <td>٥</td> <td>12</td> <td>2,950</td> <td>2</td> <td>14,547</td> <td>44,931</td> <td>31</td>	14	16		11,597	129	3.62	41,981	53	0	0	0	٥	12	2,950	2	14,547	44,931	31
75 119 27.813 309 2.90 80.658 56 0 0 0 0 28 7.075 103 82 19.253 214 3.6 60.288 42 0 0 0 0 20 4.888 112 82 19.253 214 3.14 60.458 42 0 0 0 0 0 20 4.888 112 82 19.253 214 3.14 60.458 42 0	15	32		10,235	114	3.62	37,051	56	0	0	0	0	16	4,050	က	14,285	41,101	29
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112 75 12,074 134 3.62 43,707 30 0 0 0 0 19 47.78 173 181 42,457 472 2.74 116,332 81 0 0 0 0 0 43 10,800 124 185 15,896 477 2.74 116,332 81 0 0 0 0 0 0 43 10,800 124 185 31,548 351 2.90 91,489 64 0 0 0 0 0 32 8,025 104 133 21,576 240 3.14 67,749 47 0 0 0 0 0 0 32 8,036 25 90 21,11 235 3.44 66,287 46 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 <	18	142		19,253	214	3.14	60,455	42	0	0	0	0	20	4,898	3	24,151	65,352	45
173 181 42,457 472 2.74 116,332 81 0 0 0 0 43 10,800 124 98 15,866 177 3.62 57,544 40 0 0 0 0 25 6,290 174 186 31,586 177 3.62 57,544 40 0 0 0 0 34 8,538 104 133 21,576 240 3.14 67,749 47 0 0 0 0 34 8,538 127 82 13,205 147 3.62 47,801 33 0 0 0 0 34 8,538 127 82 13,205 147 3.62 47,801 33 0 0 0 0 0 37 16,870 109,135 91 14,027 3.44 66,287 46 0 0 0 0 0 0 0	19	112		12,074	134	3.62	43,707	ဇ္တ	0	0	0	0	19	4,778	3	16,851	48,484	8
124 98 15,896 177 3.62 57,544 40 0 0 0 0 25 6,290 72 135 31,548 351 2.90 91,489 64 0 0 0 0 2.90 8,025 104 133 21,576 240 3.14 67,749 47 0 0 0 0 27 6,870 23 115 27,077 300 2.90 78,321 54 0 0 0 0 27 6,870 25 90 21,11 235 3.44 60 0 0 0 27 6,870 105,135 91 14,708 163 3.62 53,244 37 0 0 0 0 27 6,85 25 90 21,11 235 3.62 53,244 37 0 0 0 0 21 5,255 24 132	20	173		42,457	472	2.74	116,332	81	0	0	0	0	43	10,800	8	53,257	127,132	88
72 135 31,548 351 2.90 91,489 64 0 0 0 34 8,258 104 133 21,576 240 3.14 61,749 47 0 0 0 0 34 8,538 23 13,576 240 3.14 61,749 47 0 0 0 0 27 6,870 25 80 21,111 235 3.44 66,287 46 0 0 0 0 21 5,865 25 90 21,111 235 3.42 66,287 46 0 0 0 21 5,865 24 133 31,027 345 2.90 89,788 62 0 0 0 21 5,865 24 133 31,027 345 2.90 89,732 60 0 0 0 21 5,865 25 91 14,708 168 36 <td>21</td> <td>124</td> <td></td> <td>15,896</td> <td>177</td> <td>3.62</td> <td>57,544</td> <td>9</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>55</td> <td>6,290</td> <td>4</td> <td>22,186</td> <td>63,834</td> <td>44</td>	21	124		15,896	177	3.62	57,544	9	0	0	0	0	55	6,290	4	22,186	63,834	44
104 133 21,576 240 3.14 67,749 47 0 0 0 34 8,538 23 115 27,007 300 2.90 78,321 54 0 0 0 0 27 6,870 25 115 27,007 300 2.90 78,321 54 0 0 0 0 27 6,870 25 80 21,110 235 3.44 66,287 46 0 0 0 0 21 5,865 24 133 31,027 345 2.90 89,978 62 0 0 0 0 23 5,865 24 133 31,027 345 2.90 89,978 62 0 0 0 0 0 23 5,865 35 91 14,708 163 362 53,244 37 0 0 0 0 0 0 0	22	72		31,548	351	2.90	91,489	49	0	0	0	0	33	8,025	9	39,573	99,514	69
23 115 27,007 300 2.90 78,321 54 0 0 0 0 27 6,870 127 82 13,205 147 3.62 47,801 33 0 0 0 0 21 5,225 25 90 21,111 235 3.44 66,287 46 0 0 0 0 21 5,370 109,135 91 14,822 365 3.62 36,665 37 0 0 0 0 23 5,820 24 133 31,708 163 3.62 53,244 37 0 0 0 0 0 0 0 32 7,820 35 91 14,708 163 3.62 53,244 37 0 0 0 0 0 0 32 7,820 88 135 21,848 243 3.14 68,602 48 0 0	23	104		21,576	240	3.14	67,749	47	0	0	0	0	8	8,538	9	30,113	76,286	53
127 82 13,205 147 3.62 47,801 33 0 0 0 21 5,225 25 90 21,111 235 3.44 66,287 46 0 0 0 21 5,225 109,135 91 14,822 3.62 53,656 37 0 0 0 0 23 7,883 24 133 31,027 346 53,244 37 0 0 0 0 32 7,893 82 126 29,563 3.62 53,244 37 0 0 0 32 7,893 88 135 21,848 243 3.14 68,602 48 0 0 0 33 8,645 88 135 21,848 243 3.14 68,602 48 0 0 0 0 33 8,645 70 155 36,167 402 27 48 0 <td>24</td> <td>23</td> <td></td> <td>27,007</td> <td>300</td> <td>2.90</td> <td>78,321</td> <td>4</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>27</td> <td>6,870</td> <td>2</td> <td>33,877</td> <td>85,191</td> <td>59</td>	24	23		27,007	300	2.90	78,321	4	0	0	0	0	27	6,870	2	33,877	85,191	59
25 90 21,111 235 3.14 66,287 46 0 0 0 21 5,370 109,135 91 14,822 165 3.62 53,656 37 0 0 0 0 23 5,865 24 133 31,027 3.62 53,644 37 0 0 0 0 23 7,893 85 91 4,182 2.90 89,978 62 0 0 0 0 23 7,893 82 126 29,563 3.28 2.90 85,732 60 0 0 0 33 7,520 88 135 21,848 243 3.14 68,602 48 0 0 0 33 8,645 88 135 21,848 243 3.14 68,602 48 0 0 0 33 8,185 58 127 20,515 228 3.14 6	52	127		13,205	147	3.62	47,801	33	0	0	0	٥	7	5,225	4	18,430	53,026	37
109,135 91 14,822 165 3.65 37 0 0 0 23 5,865 24 133 31,027 345 2.90 89,978 62 0 0 0 0 32 5,865 35 91 14,708 162 2.90 89,478 62 0 0 0 0 23 5,820 62 126 29,633 36,724 37 0 0 0 0 0 30 7,820 88 135 21,848 243 3.14 68,602 48 0 0 0 30 35 8,645 70 155 36,167 402 2.74 99,096 69 0 0 0 37 9,200 58 127 20,515 228 3.14 64,416 45 0 0 0 32 8,18 69,133 334 78,211 36 246 <td>26</td> <td>53</td> <td></td> <td>21,111</td> <td>235</td> <td>3.14</td> <td>66,287</td> <td>46</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>73</td> <td>5,370</td> <td>4</td> <td>26,481</td> <td>71,657</td> <td>20</td>	26	53		21,111	235	3.14	66,287	46	0	0	0	0	73	5,370	4	26,481	71,657	20
24 133 31,027 345 2.90 89,978 62 0 0 0 32 7,893 35 91 14,708 163 3.62 53,244 37 0 0 0 0 23 7,893 62 126 29,563 3.62 53,244 37 0 0 0 0 30 7,520 88 136 21,863 23,34 66,02 48 0 0 0 0 35 8,645 58 127 20,515 2.24 99,088 69 0 0 0 37 9,200 69,133 334 78,211 869 2.46 192,400 134 0 0 0 33 8,185 61,134 129 20,849 232 3.14 66,467 45 0 0 0 0 32 8,185 61,134 129 20,849 23 3.14	27	109,135		14,822	165	3.62	53,656	37	0	0	0	0	ន	5,865	4	20,687	59,521	41
35 91 14,708 163 3.62 53,244 37 0 0 0 23 5,820 62 126 29,563 328 2.90 85,732 60 0 0 0 0 30 7,520 88 135 21,848 243 3.14 68,602 48 0 0 0 0 35 8,645 70 155 36,167 402 2.74 99,098 69 0 0 0 0 37 9,200 58 127 20,511 2.86 18,416 45 0 0 0 0 32 8,146 69,133 334 78,211 869 2.46 19,40 0 0 0 33 8,250 61,34 129 20,849 2.32 3.14 65,467 45 0 0 0 33 8,250 68 136 37,012 411 <td< td=""><td>28</td><td>24</td><td></td><td>31,027</td><td>345</td><td>2.90</td><td>89,978</td><td>62</td><td>0</td><td>0</td><td>0</td><td>0</td><td>32</td><td>7,893</td><td>2</td><td>38,919</td><td>97,871</td><td>88</td></td<>	28	24		31,027	345	2.90	89,978	62	0	0	0	0	32	7,893	2	38,919	97,871	88
62 126 29,563 328 2.90 85,732 60 0 0 0 0 30 7,520 88 135 21,848 2.49 85,732 60 0 0 0 0 35 8,645 70 155 36,167 402 2.74 99,098 69 0 0 0 0 37 9,200 58 127 20,515 228 3.14 64,416 45 0 0 0 0 32 8,118 69,133 334 78,211 886 2.46 192,400 134 0 0 0 0 19,855 61,134 129 20,849 232 3.14 65,467 45 0 0 0 0 19,855 68 158 37,012 411 2.74 101,414 70 0 0 0 38 9,415 67 333 77,966	59	જ		14,708	163	3.62	53,244	37	0	0	0	٥	ន	5,820	4	20,528	59,064	41
88 135 21,848 243 3.14 68,602 48 0 0 0 35 8,645 70 155 36,167 402 2.74 99,098 69 0 0 0 37 9,200 58 127 20,515 228 3.14 64,416 45 0 0 0 0 32 8,118 69,133 334 78,211 868 232 3.14 64,416 45 0 0 0 0 80 19,855 68 138 37,012 411 2.74 101,414 70 0 0 0 38 9,415 67 333 77,966 866 2.46 191,795 133 0 0 0 0 29 7,288 67 333 77,966 866 2.46 191,795 133 0 0 0 79 19,833 50 105	8	62		29,563	328	2.90	85,732	8	0	0	٥	0	8	7,520	2	37,083	93,252	92
70 155 36.167 402 2.74 99.098 69 0 0 0 37 9.200 58 127 20,515 228 3.14 64.16 45 0 0 0 0 32 8,118 69,133 334 78,211 869 2.46 192,400 134 0 0 0 0 19,895 61,134 129 20,849 2.24 10,1414 70 0 0 0 33 8,155 68 156 37,012 4.11 2.74 10,1414 70 0 0 0 38 9,415 51 144 18,417 205 3.14 57,829 40 0 0 0 38 9,415 67 333 77,966 866 2.46 191,795 133 0 0 0 0 79 19,833 50 105 105 0 0	3	88		21,848	243	3.14	68,602	48	0	0	٥	0	33	8,645	9	30,493	77,247	2
58 127 20,515 228 3.14 64,416 45 0 0 0 0 32 8,118 69,133 334 78,211 869 2.46 192,400 134 0 0 0 0 0 33 8,250 61,134 129 20,849 2.74 65,467 45 0 0 0 33 8,250 68 158 37,012 411 2.74 101,414 70 0 0 0 38 9,415 51 114 18,417 205 3.14 57,829 40 0 0 0 29 7,288 67 333 77,966 866 2.46 191,795 133 0 0 0 79 19,833 50 105 17,090 190 362 61,866 43 0 0 0 0 79 19,833 52 80 13,015	35	2		36,167	402	2.74	860,66	69	0	0	0	٥	37	9,200	9	45,367	108,298	22
69,133 334 78,211 869 2.46 192,400 134 0 0 0 0 80 19,895 61,134 129 20,849 232 3.14 65,467 45 0 0 0 0 33 8,250 68 158 37,012 411 2.74 101,144 70 0 0 0 38 9,415 51 144 18,477 254 314 57,829 40 0 0 0 29 7,288 67 333 77,966 866 2.46 191,785 133 0 0 0 79 19,833 50 105 17,090 190 3.62 61,866 43 0 0 0 27 6,763 52 80 13,015 145 3.62 47,115 33 0 0 0 0 21 5,150	33	28		20,515	228	3.14	64,416	45	0	0	0	0	32	8,118	Q	28,632	72,533	20
61,134 129 20,849 232 3.14 65,467 45 0 0 0 0 33 8,250 68 158 37,012 411 2.74 101,414 70 0 0 0 38 9,415 51 114 18,417 205 3.14 57,829 40 0 0 0 29 7,288 67 333 77,966 866 2.46 191,795 133 0 0 0 79 19,833 50 105 17,090 190 3.62 61,866 43 0 0 0 79 19,833 52 80 13,015 145 3.62 47,115 33 0 0 0 27 6,763	8	69,133		78,211	869	2.46	192,400	134		0	0	0	8	19,895	14	98,106	212,295	147
68 158 37,012 411 2.74 101,414 70 0 0 0 38 9,415 51 114 18,417 205 3.14 57,829 40 0 0 0 29 7,288 67 333 77,966 866 2.46 191,795 133 0 0 0 79 19,833 50 105 17,090 190 3.62 61,866 43 0 0 0 27 6,763 52 80 13,015 145 3.62 47,115 33 0 0 0 27 6,763	8	61,134	129	20,849	232	3.14	65,467	45	0	0	0	0	33	8,250	9	29,099	73,717	51
51 114 18,417 205 3.14 57,829 40 0 0 0 0 29 7,288 67 333 77,966 866 2.46 191,795 133 0 0 0 0 79 19,833 50 105 17,090 190 3.62 61,866 43 0 0 0 27 6,763 52 80 13,015 145 3.62 47,115 33 0 0 0 27 6,753	36	99	158	37,012	411	2.74	101,414	2	0	0	0	0	38	9,415	7	46,427	110,829	77
67 333 77,966 866 2.46 191,795 133 0 0 0 0 79 19,833 50 105 17,090 190 3.62 61,866 43 0 0 0 27 6,763 52 80 13,015 145 3.62 47,115 33 0 0 0 21 5,150	37	51	114	18,417	202	3.14	57,829	40	0	0	0	0	83	7,288	2	25,704	65,117	45
50 105 17,090 190 3.62 61,866 43 0 0 0 0 27 6,763 52 80 13,015 145 3.62 47,115 33 0 0 0 21 5,150	38	29	333	996'22	998	2.46	191,795	133	0	0	0	0	79	19,833	14	92,798	211,628	147
52 80 13,015 145 3.62 47,115 33 0 0 0 0 21 5,150	39	50	105	17,090	190	3.62	61,866	43	0	0	0	0	27	6,763	5	23,853	68,629	48
	4	52	88	13,015	145	3.62	47,115	33	0		0	0	21	5,150	4	18,165	52,265	36

MERRILL RANCH - PULTE DEVELOPMENT WEST OF FELIX ROAD WASTEWATER LOADS 10/20/2004

				Residential	ential				Commercial	nercial			Infiltration		Design	Design Flows (Maximum)	(mn
i	į	;	Ave. Day		Peak	ak Day		Avera	Average Day	Peak Day	Day	(no design	(no design peaking factors applied)	s applied)	Treatment	Collection	uo
Parcel	Į		MOLE	Don	Daaking	Flow	>	Area	Flow	Flow	*	Area	Flow	W	Flow	Flow (System Loading)	Loading)
		E	(pdb)	(pers.)	Factor	(pdb)	(mdb)	(acre)	(pdb)	(pdB)	(mdb)	(acre)	(pdb)	(mdB)	(pdb)	(pd6)	(mdg)
43	53,136	96	15,605	173	3.62	56,492	39	0	0	0	0	25	6,175	4	21,780	62,667	44
45	49	86	15,795	176	3.62	57,178	40	0	0	0	0	22	6,250	4	22,045	63,428	44
47	48	124	20,142	224	3.14	63,245	44	0	0	0	0	32	7,970	9	28,112	71,215	49
49	45	7.1	11,436	127	3.62	41,397	29	0	0	0	0	18	4,525	3	15,961	45,922	32
51	98	196	31,678	352	2.90	91,868	64	0	0	0	0	20	12,535	6	44,213	104,403	23
23	47	145	23,427	260	3.14	73,561	51	0	0	0	0	37	9,270	9	32,697	82,831	28
99	46	154	24,931	277	3.14	78,283	54	0	0	0	0	39	9,865	7	34,796	88,148	61
٧	36	120	19,459	312	2.90	56,432	39	0	0	0	0	29	7,150	5	26,609	63,582	44
8	25	22	4,001	64	3.62	14,483	10	0	0	0	0	9	1,470	1	5,471	15,953	11
2	99	0	0	0	0	0	0	22.56	22,560	67,680	47	23	5,640	4	28,200	73,320	51
Q	82	0	0	0	0	0	0	12.01	12,010	36,030	25	12	3,003	2	15,013	39,033	27
Ш	108	0	0	0	0	0	0	6.92	6,920	20,760	14	7	1,730	,	8,650	22,490	16
4	83	0	0	0	0	0	0	10.00	10,000	30,000	21	10	2,500	2	12,500	32,500	23
9	78	0	0	0	0	0	0	18.00	18,000	54,000	38	18	4,500	3	22,500	58,500	41
I	139	0	0	0	0	0	0	12.02	12,020	36,060	52	12	3,005	2	15,025	39,065	27
_	139	0	0	0	0	0	0	0.50	500	1,500	1	-	125	0.1	625	1,625	1
f	100	0	0	0	0	0	0	0.50	200	1,500	-	,	125	0.1	625	1,625	1
¥	138	0	0	0	0	0	0	2.00	2,000	6,000	4	2	200	0.3	2,500	6,500	2
	26	0	0	0	0	0	0	17.03	17,030	51,090	32	17	4,258	3	21,288	55,348	38
Σ	71	0	0	0	0	0	0	16.00	16,000	48,000	33	16	4,000	3	20,000	52,000	36
Z	60	0	0	0	0	0	0	5.63	5,630	16,890	12	9	1,408	1	7,038	18,298	13
0	60	0	0	0	0	0	0	1.96	1,960	5,880	4	2	490	0.3	2,450	6,370	4
Д	100	0	0	0	0	0	0	18.04	18,040	54,120	38	18	4,510	3	22,550	58,630	41
To	Totals	6,011	1,177,234	13,196		3,566,336	2,477	143	143,170	429,510	298	1,630	407,483	283	1,727,886	4,403,329	3,058

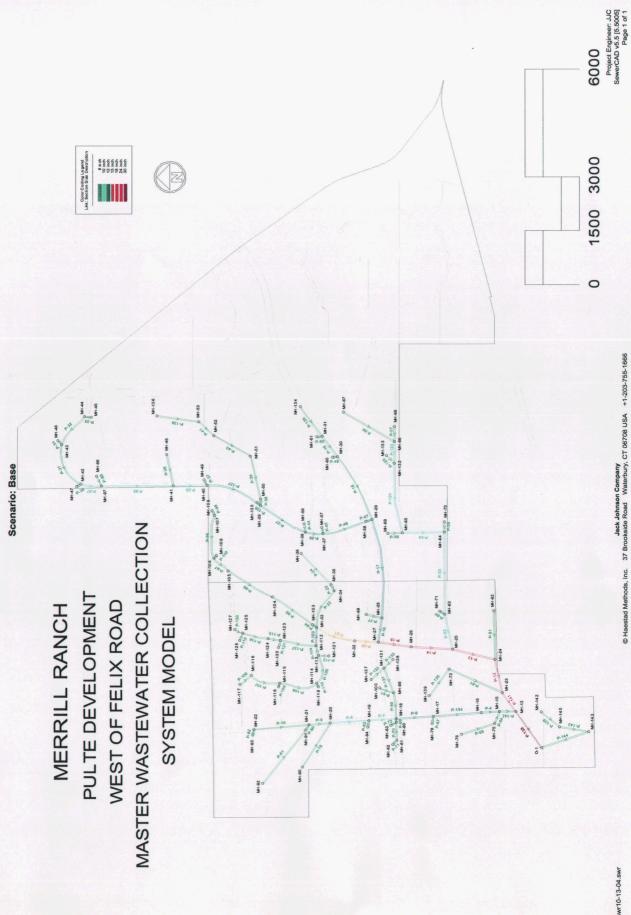
Design Flow (gpm)
All Parcels 3,058

Wastewater System Design Criteria:

- gpd per person (residentail areas requiring sewers) 90
 - persons/D.U. (all Family Community Residences) 8,
- persons/D.U. (all Adult Community Residences) peaking factor (varies per contributing residential population density)
 - gpd per acre (all commercial and school areas) - 1,000
 - peaking factor (all commercial and school areas) 3.0
- gpd per acre (for wet weather flow infiltration and inflow)

Note that all calculations are based upon "Johnson Utilities Company Design Guide and Standard Detaits" May 2003.

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Title: MERRILL RANCH y:\...\sewercadi742-mstrswr10-13-04.swr 10/20/04 09:04:42 AM

Manhole Report

Label	Rim Elevation (ft)	Sump Elevation (ft)	Headloss Coefficient	Sanitary Pattern Load Base Flow (gpm)	Total Flow (gpm)	Velocity Out (ft/s)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Energy Grade Line In (ft)	Energy Grade Line Out (ft)
MH-13	1,456.00	1,439.46	0.90	0.0	2,925.0	2.40	1,440.89	1,440,81	1,440,98	1,440.90
MH-15	1,458.00	1,448.32	0.80	0.0	674.0	3.64	1,449.00	1,448.84	1,449.21	1,449.05
MH-16	1,460.00	1,449.96	0.80	31.0	552.0	2.72	1,450.61	1,450.52	1,450.73	1,450.63
MH-17	1,470.00	1,454.36	1.00	0.0	521.0	2.69	1,455.01	1,454.90	1,455.12	1,455.01
MH-18	1,475.00	1,457.75	1.00	0.0	480.0	2.63	1,458.37	1,458.26	1,458.48	1,458.37
MH-19	1,478.00	1,468.12	0.80	0.0	355.0	3.13	1,468.63	1,468.51	1,468.79	1,468.66
MH-20	1,482.00	1,471.67	0.80	0.0	263.0	2.27	1,472.13	1,472.07	1,472.21	1,472.15
MH-21	1,485.00	1,476.04	0.80	0.0	199.0	2.78	1,476.45	1,476,35	1,476.57	1,476.47
MH-22	1,494.00	1,481.14	0.60	0.0	56.0	1.51	1,481.35	1,481.33	1,481.39	1,481.37
MH-23	1,454.00	1,439.94	1.00	59.0	2,251.0	2.17	1,441.39	1,441.32	1,441.47	1,441.39
MH-24	1,460.00	1,440.67	1.00	68.0	2,095.0	2.12	1,442.06	1,441.99	1,442.13	1,442.06
MH-25	1,459.00	1,447.75	1.00	50.0	1,962.0	4.55	1,448.87	1,448.55	1,449.19	1,448.87
MH-26	1,462.00	1,450.54	0.80	38.0	1,430.0	3.09	1,451.51	1,451.39	1,451.66	1,451.54
MH-27	1,465.37	1,452.28	0.80	0.0	1,392.0	2.78	1,451.31	1,451.39	1,451.60	1,451.34
MH-28	1,467.00	1,454.54	0.80	0.0	744.5	2.76	1,455.26	1,455.10	1,455.46	1,455.35
MH-29	1,490.00	1,475.55	0.80	0.0	690.5	3.67	1,476.24	1,476.08	1,476.45	1,476.29
MH-30	1,497.00	1,488.97	0.80	0.0	68.0	2.02	1,489.20	1,489.15	1,489.26	1,489.21
MH-31	1,503.00	1,492.50	0.60	0.0	51.0	1.70	1,492.69	1,492.66	1,492.74	1,492.71
MH-32	1,466.00	1,453.50	0.80	29.0	647.5	2.31	1,454.20	1,454.13	1,454.28	1,454.22
MH-33	1,470.00	1,455.66	1.00	0.0	618.5	2.28	1,456.36	1,456.28	1,456.44	1,456.36
MH-34	1,477.00	1,461.50	0.60	0.0	85.0	1.97	1,461.75	1,461.71	1,461.81	1,461.77
MH-35	1,481.00	1,462.49	0.80	41.0	85.0	1.97	1,462.75	1,462.70	1,462.81	1,462.76
MH-36	1,483.00	1,468.43	0.80	44.0	44.0	1.63	1,468.62	1,468.58	1,468.66	1,468.62
MH-37	1,487.00	1,478.23	0.80	0.0	572.5	2.21	1,478.98	1,478.92	1,479.06	1,479.00
MH-38	1,488.00	1,479.17	0.80	0.0	561.5	2.20	1,479.91	1,479.85	1,479.99	1,479.92
MH-39	1,492.56	1,481.92	0.80	0.0	510.5	2.16	1,482.61	1,482.56	1,482.69	1,482.63
MH-40	1,497.50	1,485.01	0.80	0.0	317.0	1.93	1,485.53	1,485.48	1,485.59	1,485.54
MH-41	1,498.32	1,487.26	0.80	0.0	273.0	2.03	1,487.76	1,487.71	1,487.82	1,487.77
MH-42	1,500.00	1,493.60	0.90	0.0	151.0	1.81	1,493.96	1,493.91	1,494.01	1,493.96
MH-43	1,505.28	1,497.93	0.90	0.0	93.0	1.74	1,498.22	1,498.18	1,498.27	1,498.23
MH-44	1,509.00	1,501.26	0.60	0.0	32.0	1.28	1,501.42	1,501.40	1,501.45	1,501.43
MH-45	1,508.50	1,501.20	0.80	32.0	32.0	1.28	1,502.07	1,502.05	1,502.10	1,502.08
MH-46	1,506.00	1,498.46	0.80	61.0	61.0	1.55	1,498.69	1,498.66	1,498.73	1,498.70
MH-47	1,500.00	1,494.02	0.80	58.0	58.0	1.53	1,494.24	1,494.21	1,494.28	1,494.25
MH-48	1,502.50	1,490.21	0.80	49.0	49.0	1.45	1,490.41	1,490.39	1,490.45	1,490.42
MH-49	1,498.68	1,485.55	0.80	44.0	44.0	1.42	1,485.74	1,485.72	1,485.77	1,485.75
MH-50	1,494.23	1,483.06	0.80	48.0	173.0	2.64	1,483.44	1,483.35	1,483.55	1,483.46
MH-51	1,504.00	1,491.29	0.90	45.0	125.0	2.41	1,491.62	1,491.53	1,491.71	1,491.62
MH-52	1,507.00	1,499.09	0.80	36.0	80.0	2.12	1,499.34	1,499.28	1,499.41	1,499.35
MH-53	1,508.00	1,500.94	0.80	22.0	44.0	1.41	1,501.13	1,501.11	1,501.16	1,501.14
MH-56	1,489.00	1,479.93	0.80	51.0	51.0	1.46	1,480.14	1,480.11	1,480.17	1,480.15
MH-57	1,489.00	1,479.10	0.80	11.0	11.0	1.08	1,479.19	1,479.18	1,479.21	1,479.20
MH-58	1,489.00	1,475.89	0.80	50.0	622.5	2.26	1,476.68	1,476.62	1,476.76	1,476.70
MH-60	1,497.00	1,489.44	0.80	17.0	17.0	1.06	1,489.56	1,489.55	1,489.58	1,489.56
MH-61	1,503.50	1,492.99	0.80	25.5	25.5	1.19	1,493.14	1,493.12	1,493.16	1,493.14
MH-62	1,468.00	1,445.15	0.80	65.0	65.0	1.57	1,445.39	1,445.36	1,445.43	1,445.40
MH-63	1,468.00	1,460.00	9.00	0.0	482.0	3.47	1,462.14	1,460.46	1,462.33	1,460.65
MH-64	1,485.00	1,467.50	0.80	0.0	446.0	2.56	1,468.14	1,468.06	1,468.24	1,468.16
MH-65	1,489.50	1,470.27	0.80	0.0	371.0	2.17	1,470.88	1,470.82	1,470.95	1,470.89
MH-66	1,494.00	1,477.93	0.80	0.0	224.0	2.17	1,478.35	1,478.30	1,478.43	1,478.37
MH-67	1,495.00	1,483.33	0.80	147.0	147.0	1.96	1,483.70	1,483.65	1,483.76	1,483.71
MH-68	1,494.00	1,479.29	0.80	77.0	77.0	1.65	1,479.55	1,403.03	1,479.59	1,479.56
MH-69	1,490.00	1,473.23	0.80	73.5	77.5	1.89	1,473.54	1,473.52	1,479.60	1,479.55

Title: MERRILL RANCH

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Manhole Report

Label	Rim Elevation (ft)	Sump Elevation (ft)	Headloss Coefficient	Sanitary Pattern Load Base Flow	Total Flow (gpm)	Velocity Out (ft/s)	Hydraulic Grade Line In	Hydraulic Grade Line Out	Energy Grade Line In	Energy Grade Line Out
	(11)	(19		(gpm)		(103)	(ft)	(ft)	(ft)	(ft)
MH-70	1,481.00	1,468.47	0.80	75.0	75.0	1.63	1,468.73	1,468.69	1,468.77	1,468.73
MH-71	1,468.00	1,460.54	0.80	36.0	36.0	0.23	1,462.15	1,462.15	1,462.15	1,462.15
MH-72	1,460.00	1,445.28	0.80	69.0	97.0	1.76	1,445.57	1,445.54	1,445.62	1,445.58
MH-75	1,461.00	1,449.72	0.80	61.0	122.0	1.98	1,450.05	1,450.00	1,450.11	1,450.06
MH-76	1,468.00	1,452.95	0.80	61.0	61.0	1.54	1,453.18	1,453.15	1,453.22	1,453.19
MH-78	1,472.00	1,455.04	0.80	41.0	41.0	1.38	1,455.23	1,455.20	1,455.26	1,455.23
MH-80	1,477.00	1,458.28	0.80	0.0	50.0	1.69	1,458.48	1,458.44	1,458.52	1,458.49
MH-81	1,480.00	1,460.74	0.60	0.0	27.0	1.41	1,460.88	1,460.86	1,460.91	1,460.89
MH-82	1,480.00	1,461.60	0.80	27.0	27.0	1.41	1,461.74	1,461.72	1,461.78	1,461.75
MH-83	1,478.00	1,459.14	0.80	23.0	23.0	1.34	1,459.27	1,459.25	1,459.30	1,459.28
MH-88	1,470.00	1,456.05	0.80	54.0	54.0	1.49	1,456.27	1,456.24	1,456.30	1,456.27
MH-90	1,494.00	1,486.14	0.80	64.0	64.0	1.99	1,486.36	1,486.31	1,486.42	1,486.37
MH-91	1,486.00	1,476.64	0.80	73.0	143.0	1.94	1,477.00	1,476.96	1,477.06	1,477.02
MH-92	1,500.00	1,482.90	0.80	70.0	70.0	1.60	1,483.15	1,483.11	1,483.19	1,483.15
MH-93	1,495.00	1,481.68	0.80	56.0	56.0	1.50	1,481.90	1,481.87	1,481.93	1,481.91
MH-94	1,479.00	1,468.73	0.80	92.0	92.0	1.72	1,469.02	1,468.98	1,469.06	1,469.03
MH-97	1,500.00	1,492.03	0.80	0.0	224.0	1.93	1,492.48	1,492.43	1,492.53	1,492.49
MH-98	1,500.00	1,493.06	0.80	73.0	73.0	1.62	1,493.31	1,493.28	1,493.35	1,493.32
MH-99	1,471.00	1,460.11	0.80	0.0	75.0	1.63	1,460.37	1,460.33	1,460.41	1,460.37
MH-100	1,472.00	1,461.47	0.80	42.0	42.0	1.39	1,461.66	1,461.64	1,461.69	1,461.67
MH-103	1,471.00	1,456.38	0.80	46.0	135.5	2.23	1,456.72	1,456.65	1,456.79	1,456.73
MH-104	1,475.00	1,463.13	0.80	53.0	89.5	2.00	1,463.40	1,463.35	1,463.46	1,463.41
MH-105	1,485.00	1,470.25	0.60	0.0	36.5	1.54	1,470.41	1,470.39	1,470.45	1,470.43
MH-106	1,483.00	1,472.85	0.80	0.0	36.5	1.54	1,473.02	1,472.99	1,473.06	1,473.03
MH-107	1,492.00	1,478.92	0.60	0.0	16.0	1.21	1,479.03	1,479.01	1,479.05	1,479.04
MH-108	1,492.00	1,479.73	0.80	16.0	16.0	1.21	1,479.84	1,479.82	1,479.86	1,479.85
MH-109	1,482.00	1,473.25	0.80	20.5	20.5	1.13	1,473.38	1,473.37	1,473.40	1,473.39
MH-112	1,470.00	1,456.88	0.80 1.00	34.0 40.0	398.0 201.0	2.23 2.10	1,457.45	1,457.38	1,457.52	1,457.46
MH-113 MH-114	1,470.00 1,476.00	1,457.81 1,461.96	0.80	40.0 0.0	133.0	2.10	1,458.27 1,462.29	1,458.20° 1,462.23	1,458.34 1,462.37	1,458.27 1,462.31
MH-115	1,479.00	1,467.32	0.80	0.0	86.0	1.97	1,462.29	1,462.23	1,462.57	1,462.51
MH-116	1,481.00	1,471.62	0.60	0.0	39.0	1.57	1,407.38	1,407.33	1,471.83	1,471.80
MH-117	1,484.00	1,472.95	0.80	39.0	39.0	1.36	1,473.13	1,473.11	1,473.16	1,473.14
MH-118	1,480.00	1,467.70	0.80	47.0	47.0	1.43	1,467.90	1,467.88	1,467.93	1,467.91
MH-119	1,477.00	1,462.34	0.80	47.0	47.0	1.44	1,462.54	1,462.51	1,462.57	1,462.55
MH-121	1,469.00	1,458.74	0.80	28.0	28.0	1.23	1,458.89	1,458.88	1,458.92	1,458.90
MH-123	1,473.30	1,460.16	0.80	0.0	163.0	2.01	1,460.55	1,460.50	1,460.62	1,460.57
MH-124	1,475.00	1,461.32	0.80	44.0	129.0	1.89	1,461.66	1,461.62	1,461.72	1,461.67
MH-125	1,476.00	1,463.69	0.80	0.0	85.0	1.69	1,463.96	1,463.93	1,464.01	1,463.97
MH-127	1,477.00	1,464.49	0.80	37.0	37.0	1.34	1,464.67	1,464.65	1,464.70	1,464.67
MH-128	1,476.40	1,464.40	0.80	48.0	48.0	1.44	1,464.60	1,464.58	1,464.64	1,464.61
MH-130	1,474.10	1,460.81	0.80	34.0	34.0	1.30	1,460.98	1,460.96	1,461.01	1,460.99
MH-131	1,472.00	1,462.59	0.80	0.0	33.0	1.29	1,462.76	1,462.74	1,462.78	1,462.76
MH-132	1,490.00	1,475.93	0.80	0.0	297.5	2.23	1,476.44	1,476.38	1,476.52	1,476.45
MH-133	1,485.00	1,476.94	0.80	73.5	73.5	1.62	1,477.19	1,477.16	1,477.23	1,477.20
MH-134	1,500.00	1,495.87	0.80	25.5	25.5	1.20	1,496.02	1,496.00	1,496.04	1,496.02
MH-135	1,493.00	1,482.17	0.80	20.5	337.5	1.70	1,482.76	1,482.72	1,482.80	1,482.77
MH-136	1,509.00	1,504.80	0.80	22.0	22.0	1.15	1,504.94	1,504.92	1,504.96	1,504.94
MH-137	1,471.00	1,464.20	0.80	28.0	28.0	1.24	1,464.35	1,464.33	1,464.38	1,464.36
MH-138	1,470.00	1,463.72	0.80	5.0	5.0	0.74	1,463.79	1,463.78	1,463.79	1,463.79
MH-139	1,468.00	1,449.91	0.80	28.0	28.0	1.43	1,450.06	1,450.03	1,450.09	1,450.06
MH-140	1,455.00	1,445.76	0.80	0.0	45.0	1.41	1,445.96	1,445.93	1,445.99	1,445.96
MH-142	1,455.00	1,447.93	0.80	45.0	45.0	1.41	1,448.13	1,448.10	1,448.16	1,448.13

Title: MERRILL RANCH

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Project Engineer: JJC SewerCAD v5.5 [5.5005]

0-13-04.swr Jack Johnson Company
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Manhole Report

Label	Rim Elevation (ft)	Sump Elevation (ft)	Headloss Coefficient	Sanitary Pattern Load Base Flow (gpm)	Total Flow (gpm)	Velocity Out (ft/s)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Energy Grade Line In (ft)	Energy Grade Line Out (ft)
MH-143	1,449.00	1,443.10	0.80	88.0	133.0	1.92	1,443.45	1,443.40	1,443.51	1,443.46

Gravity Pipe Report

Label	Length (ft)	Section Size	Mannings n	Constructed Slope (ft/ft)	Average Velocity (ft/s)	Total Flow (gpm)	Design Capacity (gpm)	Excess Design Capacity (gpm)
P-4	497.00	12 inch	0.013	0.003300	2.72	552.0	918.5	366.5
P-6	1,027.00	12 inch	0.013	0.003301	2.63	480.0	918.7	438.7
P-7	754.00	10 inch	0.013	0.013753	4.15	355.0	1,153.2	798.2
P-8	1,076.00	10 inch	0.013	0.003299	2.27	263.0	564.8	301.8
P-9	584.00	8 inch	0.013	0.007483	2.87	199.0	469.1	270.1
P-10	1,544.00	8 inch	0.013	0.003303	1.51	56.0	311.7	255.7
P-12	947.00	24 inch	0.013	0.000771	2.19	2,095.0	2,818.9	723.9
P-13	1,218.00	18 inch	0.013	0.005813	4.63	1,962.0	3,594.4	1,632.4
P-14	1,140.00	18 inch	0.013	0.002447	3.09	1,430.0	2,332.3	902.3
P-15	916.00	18 inch	0.013	0.001900	2.78	1,392.0	2,054.7	662.7
P-16	687.00	12 inch	0.013	0.003290	2.90	744.5	917.1	172.6
P-17	2,772.00	12 inch	0.013	0.007579	3.94	690.5	1,392.1	701.6
P-18	1,995.00	8 inch	0.013	0.006727	2.05	68.0	444.8	376.8
P-19	704.00		0.013	0.005014	1.70	51.0	384.0	333.0
P-20	643.00	15 inch	0.013	0.001897	2.31	647.5	1,262.9	615.4
P-21	1,138.00	15 inch	0.013	0.001898	2.28	618.5	1,263.1	644.6
P-22	1,167.00		0.013	0.005004	1.97	85.0	383.7	298.7
P-23	198.00		0.013	0.005000	1.97	85.0	383.5	298.5
P-24	1,187.00		0.013	0.005004	1.63	44.0	383.7	339.7
P-26	•	12 inch	0.013	0.003004	2.20	561.5	697.5	136.0
P-27	1,446.00		0.013	0.001903	2.16	510.5	697.3	186.8
P-29	934.00	12 inch	0.013	0.001902	2.10	273.0	482.6	209.6
P-31			0.013	0.002409				
		8 inch	1		1.74	93.0	311.9	218.9
P-32	1,015.00		0.013	0.003281	1.28	32.0	310.6	278.6
P-33		8 inch	0.013	0.003283	1.28	32.0	310.7	278.7
P-34		8 inch	0.013	0.003333	1.55	61.0	313.1	252.1
P-35	126.00		0.013	0.003333	1.53	58.0	313.1	255.1
P-36	893.00		0.013	0.003303	1.45	49.0	311.7	262.7
P-37		8 inch	0.013	0.003375	1.42	44.0	315.1	271.1
P-38	174.00		0.013	0.006552	2.64	173.0	439.0	266.0
P-39	1,235.00		0.013	0.006664	2.43	125.0	442.7	317.7
P-40	1,171.00		0.013	0.006661	2.14	80.0	442.6	362.6
P-41		8 inch	0.013	0.003304	1.41	44.0	311.7	267.7
P-44	232.00		0.013	0.003276	1.46	51.0	310.4	259.4
P-45	174.00		0.013	0.005000	1.08	11.0	383.5	372.5
P-46	1,233.00		0.013	0.001898	2.21	572.5	696.6	124.1
P-47		12 inch	0.013	0.001889	2.23	622.5	695.0	72.5
P-49	142.00	8 inch	0.013	0.003310	1.06	17.0	312.0	295.0
P-50	150.00		0.013	0.003267	1.19	25.5	310.0	284.5
P-51	1,359.00		0.013	0.003297	1.57	65.0	311.4	246.4
P-52	999.00	10 inch	0.013	0.012262	4.31	482.0	1,088.9	606.9
P-53	2,271.00	10 inch	0.013	0.003303	2.56	446.0	565.1	119.1
P-54	1,156.00	10 inch	0.013	0.002396	2.17	371.0	481.4	110.4
P-56	1,634.00	8 inch	0.013	0.003305	1.96	147.0	311.8	164.8
P-57	411.00	8 inch	0.013	0.003309	1.65	77.0	312.0	235.0
P-58	404.00	8 inch	0.013	0.005025	1.89	73.5	384.4	310.9
P-59	296.00		0.013	0.003277	1.63	75.0	310.5	235.5
P-60	162.00		0.013	0.003333	0.23	36.0	313.1	277.1
P-61	1,619.00		0.013	0.003298	1.76	97.0	311.5	214.5
P-64	364.00		0.013	0.003846	1.98	122.0	336.3	214.3
P-65	977.00		0.013	0.003306	1.54	61.0	311.8	250.8
P-67	206.00		0.013	0.003301	1.38	41.0	311.6	270.6
P-69	107.00		0.013	0.004953	1.69	50.0	381.7	331.7

Gravity Pipe Report

Label	Length (ft)	Section Size	Mannings n	Constructed Slope (ft/ft)	Average Velocity (ft/s)	Total Flow (gpm)	Design Capacity (gpm)	Excess Design Capacity (gpm)
P-70	491.00	8 inch	0.013	0.005010	1.41	27.0	383.9	356.9
P-71	172.00	8 inch	0.013	0.005000	1.41	27.0	383.5	356.5
P-72	173.00	8 inch	0.013	0.004971	1.34	23.0	382.4	359.4
P-77	455.00	8 inch	0.013	0.003319	1.49	54.0	312.4	258.4
P-79	1,447.00	8 inch	0.013	0.010000	2.32	64.0	542.3	478.3
P-80	183.00	8 inch	0.013	0.003279	1.94	143.0	310.5	167.5
P-81	1,897.00	8 inch	0.013	0.003300	1.60	70.0	311.6	241.6
P-82	166.00	8 inch	0.013	0.003253	1.50	56.0	309.3	253.3
P-83	187.00	8 inch	0.013	0.003262	1.72	92.0	309.8	217.8
P-87	587.00	10 inch	0.013	0.002675	1.81	151.0	508.5	357.5
P-88	1,987.00	10 inch	0.013	0.002401	1.93	224.0	481.8	257.8
P-89	312.00	8 inch	0.013	0.003301	1.62	73.0	311.6	238.6
P-90	718.00	8 inch	0.013	0.003287	1.63	75.0	310.9	235.9
P-91	413.00	8 inch	0.013	0.003293	1.39	42.0	311.2	269.2
P-94	145.00	8 inch	0.013	0.004966	2.23	135.5	382.2	246.7
P-95	1,350.00	8 inch	0.013	0.005000	2.00	89.5	383.5	294.0
P-96	1,424.00	8 inch	0.013	0.005000	1.54	36.5	383.5	347.0
P-97	518.00	8 inch	0.013	0.005019	1.54	36.5	384.2	347.7
P-98	1,217.00	8 inch	0.013	0.004988	1.21	16.0	383.0	367.0
P-99	161.00	8 inch	0.013	0.005031	1.21	16.0	384.7	368.7
P-100	120.00	8 inch	0.013	0.003333	1.13	20.5	313.1	292.6
P-103	507.00	12 inch	0.013	0.002406	2.23	398.0	784.4	386.4
P-104	286.00	8 inch	0.013	0.003252	2.10	201.0	309.3	108.3
P-105	829.00	8 inch	0.013	0.005006	2.23	133.0	383.7	250.7
P-106	1,075.00	8 inch	0.013	0.004986	1.97	86.0	383.0	297.0
P-107	860.00	8 inch	0.013	0.005000	1.57	39.0	383.5	344.5
P-108	402.00	8 inch	0.013	0.003308	1.36	39.0	312.0	273.0
P-109	116.00	8 inch	0.013	0.003276	1.43	47.0	310.4	263.4
P-110	114.00	8 inch	0.013	0.003333	1.44	47.0	313.1	266.1
P-112	284.00	8 inch	0.013	0.003275	1.23	28.0	310.4	282.4
P-115	353.00	8 inch	0.013	0.003286	1.89	129.0	310.9	181.9
P-116	718.00	8 inch	0.013	0.003301	1.69	85.0	311.6	226.6
P-119	216.00	8 inch	0.013	0.003287	1.44	48.0	310.9	262.9
P-121	197.00	8 inch	0.013	0.003299	1.30	34.0	311.5	277.5
P-123	608.00	10 inch	0.013	0.003289	2.17	224.0	564.0	340.0
P-124	1,947.00	10 inch	0.013	0.002907	2.23	297.5	530.2	232.7
P-125	307.00	8 inch	0.013	0.003290	1.62	73.5	311.1	237.6
P-126	1,024.00	8 inch	0.013	0.003291	1.20	25.5	311.1	285.6
P-127	1,500.00	1	0.013	0.001893	1.93	317.0	695.8	378.8
P-128	133.00	12 inch	0.013	0.001880	1.95	337.5	693.3	355.8
P-130	242.00		0.013	0.003306	1.34	37.0	311.8	274.8
P-131	751.00		0.013	0.003302	1.29	33.0	311.7	278.7
P-132	485.00		0.013	0.003320	1.24	28.0	312.5	284.5
P-133	343.00		0.013	0.003294	0.74	5.0	311.3	306.3
P-134	1,333.00		0.013	0.003301	2.69	521.0	918.7	397.7
P-135	925.00	8 inch	0.013	0.005005	1.43	28.0	383.7	355.7
P-136	1,168.00		0.013	0.003305	1.15	22.0	311.8	289.8
P-137	994.00	B.	0.013	0.003300	2.01	163.0	311.5	148.5
P-138	1,242.00		0.013	0.000773	2.40	2,925.0	5,118.0	2,193.0
P-139	658.00		0.013	0.003298	1.41	45.0	311.5	266.5
P-141	i	24 inch	0.013	0.000772	2.22	2,251.0	2,820.5	569.5
P-142		12 inch	0.013	0.019777	5.57	674.0	2,248.7	1,574.7
P-143	807.00		0.013	0.003296	1.41	45.0	311.4	266.4

Title: MERRILL RANCH

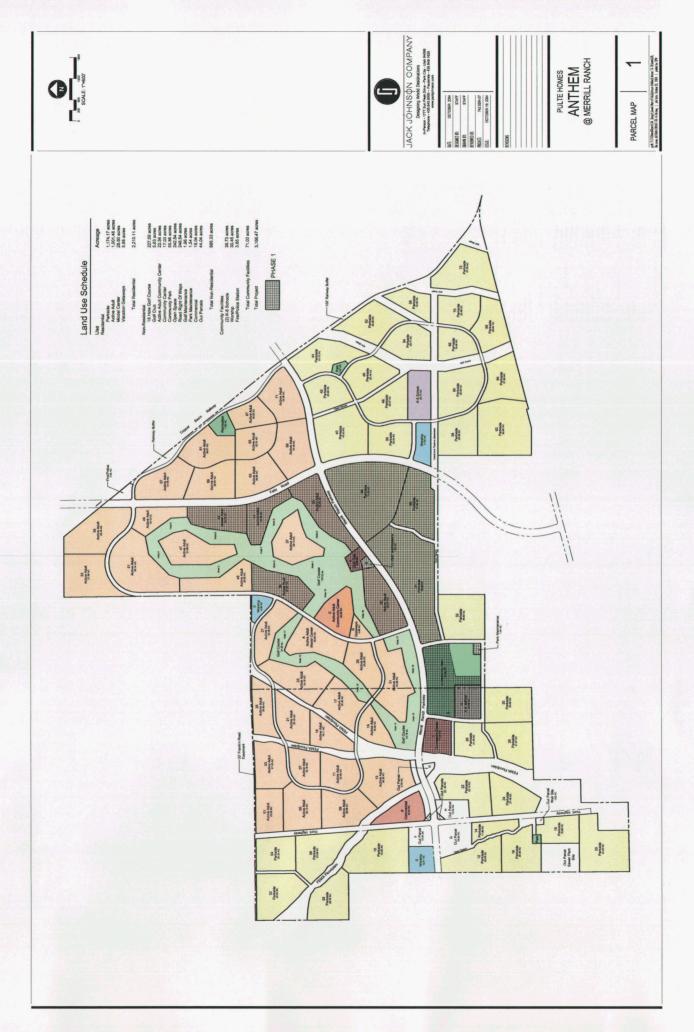
y:\...\sewercad\742-mstrswr10-13-04.swr 10/20/04 09:12:06 AM © Haestad

Gravity Pipe Report

Label	Length (ft)	Section Size	Mannings n	Constructed Slope (ft/ft)	Average Velocity (ft/s)	Total Flow (gpm)	Design Capacity (gpm)	Excess Design Capacity (gpm)
P-144	1,371.00	8 inch	0.013	0.003355	1.92	133.0	314.1	181.1

Outlet Report

Label	Rim Elevation (ft)	Sump Elevation (ft)	Total Flow (gpm)	Hydraulic Grade Line In (ft)	Hydraulic Grade Line Out (ft)	Energy Grade Line In (ft)	Energy Grade Line Out (ft)
0-1	1,460.00	1,438.50	3,058.0	1,438.50	1,438.50	1,438.50	1,438.50





JACK JOHNSON COMPANY
Designing World Destinations

In-Person -- 1777 Sun Peak Drive - Park City - Utah 84098 | Telephone - 435.645.9000 -- Facsimile - 435.649.1620

ATTACHMENT 3

FLORENCE, ARIZONA

MASTER WATER SYSTEM REPORT PULTE DEVELOPMENT WEST OF FELIX ROAD

NOVEMBER 2004

Prepared For: Pulte Homes 15333 N. Pima Road, Suite 300 Scottsdale, Arizona 85260

Prepared By: Jack Johnson Company 5745 N. Scottsdale Road, Suite 130 Scottsdale, Arizona 85250



FLORENCE, ARIZONA

MASTER WATER SYSTEM REPORT PULTE DEVELOPMENT WEST OF FELIX ROAD

NOVEMBER 2004



PROJECT ENGINEER

JACK JOHNSON COMPANY 5745 N. SCOTTSDALE ROAD, SUITE 130 SCOTTSDALE, ARIZONA 85250

> Telephone: (480) 214-0370 Facsimile: (480) 214-0356

FLORENCE, ARIZONA

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Figure 1. Project Location Map......1

Introduction

Project Location

The Pulte Development portion of Merrill Ranch West of Felix Road (the Project) lies within the jurisdiction of the Town of Florence. The Project is a 2000-acre (±) mixed-use Planned Unit Development (PUD) with low to medium-high density neighborhood housing, with several areas reserved for neighborhood businesses and commercial uses. An extensive trail network connects the lineal park system and natural desert spaces and community parks and is a part of the Open Space System. The Project is located primarily on desert scrublands, crossed by various minor drainage courses. There is a designated Federal Emergency Management Agency (FEMA) Flood Zone "A" on the western edge of Merrill Ranch. Hunt Highway runs through the property.

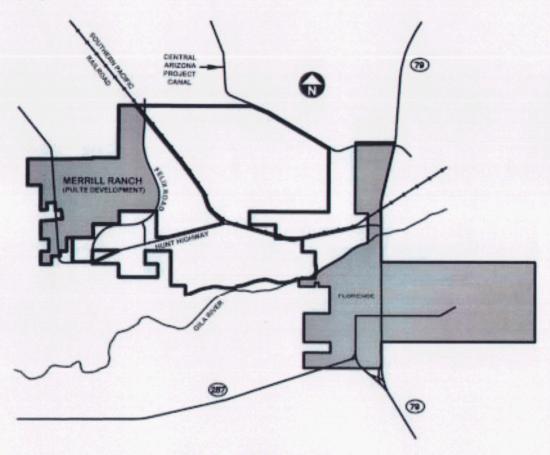


Figure 1. Project Location Map

Scope

This report presents the analysis completed for the purpose of sizing onsite water lines and estimating expected pressures and flows for the Project. The model contained herein represents the community's waterlines, i.e. lines that would participate in delivering water to the Project from offsite water lines. The water lines have been sized to deliver fire flow in addition to peak day demands. In areas of the schematic model individual water lines may have been omitted to simplify the model. Such areas share similar properties to the modeled areas and will be adequately served with a 6" line.

Peak day demands were estimated and set at various places throughout the network. The network was modeled with a fire flow at each node during peak day demands. This process was repeated for fire demands at key locations within the network. Line sizes were adjusted to maintain required flows and pressures. This process was repeated until acceptable results were obtained. This report demonstrates a network producing acceptable results according to jurisdictional criteria.

Offsite water lines and infrastructure are not part of this study. Assumptions have been made about the offsite or source system for design purposes in order to size the onsite system. These assumptions are included in the body of the report.



Jurisdictional Design Criteria

Jurisdiction

The Project lies within the jurisdictions of:

- Johnson Utilities Company
- □ Town of Florence, Arizona
- State of Arizona

Design Source Documents

The minimum design criteria against which the Project and all associated developments are measured, as pertaining to water systems, shall be in accordance with the following documents:

- Johnson Utilities Company: <u>Johnson Utilities Company Design Guide and Standard Details</u>, May 2003.
- □ Town of Florence: Development Codes Zoning Ordinance Subdivision Regulations, June 2000
- □ Arizona State: Engineering Bulletin No. 10 "Guidelines for the Construction of Water Systems" Arizona Department of Environmental Quality, May 1978
- □ Arizona State: Arizona Administrative Code R18-4-501

If, in any instance documents conflict, the most restrictive rule or regulation shall apply from the standpoint of capacity, level of service and public safety. The Engineer of Record shall bear the responsibility of interpretation of all such conflicts.

Water System Demands

Demand Calculations

Water demands were calculated using the methods prescribed by Johnson Utilities Company and were based on available planning and/or density estimations at the time of this report. A peaking factor of 2.0 was used to determine peak (or maximum) day demands with respect to average day demands. This same peaking factor shall be applied to each associated project/parcel for the purpose of designing the project water system.

See "Water System Demands" (Appendix 1)

Storage Volume

Water storage volume requirements were calculated using the methods prescribed by Johnson Utilities Company and were based on available planning and/or density estimations at the time of this report. Water equalization storage volume was calculated as 48% of peak day demands. Total required storage equals the sum of equalization and fire suppression storage.

See "Water System Demands" (Appendix 1)



Fire Flow

Residential and commercial fire flows were calculated based on a peak day demand plus a fire flow of 1,000 gpm for 2-hrs per Rural Metro Fire Department Requirements. Commercial & school facilities were assumed to have fire suppression sprinklers when needed to be able to utilize the available 1,000 gpm for 2-hrs. Additional fire suppression storage may otherwise need to be provided by developers for larger buildings not covered by 1,000 gpm for 2-hrs. The calculated 120,000-gallon fire suppression storage was assumed to be included within the existing system.

See "Water System Demands" (Appendix 1)

Source

Development of the source of the Project's water is not specifically this report's concern. The electronic water model contained herein includes two reservoirs set at an elevation to provide a sufficient hydraulic grade to pressurize the entire system. In the actual system, these reservoirs will be groundwater wells with storage tanks and booster pumps. They will be designed to charge the transmission water line network to the design hydraulic grade of the reservoirs in the water model.

See Appendix 2. Hydraulic Model Output Data

Pressure Zones

The Project has been designed to have a single pressure zone.

List of Design Parameters

- □ Well/Pump 1- Felix Road Water System Hydraulic Grade (feet): 1625
- Well/Pump 2- Rancho Sendero Water System Hydraulic Grade (feet):
 1625
- ☐ Maximum Commercial Fire Flow = 1000 gpm
- □ Maximum Residential Fire Flow = 1000 gpm
- ☐ Maximum Fire Flow from any single hydrant = 1000 gpm
- ☐ Max velocity allowed during fire flow = 10 fps
- □ Total Fire Flow = Peak Day Demand + Needed Fire Flow
- ☐ Minimum Residual Pressure during Peak Day + Fire Flow = 20 psig
- ☐ Minimum System Pressure during Peak Day + Fire Flow = 20 psig
- ☐ Maximum System Pressure during Peak Day Flow = 80 psi
- ☐ Minimum System Pressure during Peak Day Flow = 40 psi
- ☐ Minimum System Pressure during Peak Hour Flow = 40 psi
- □ Hazen-Williams Roughness "C" Factor = 150 (PVC)
- □ Water Temperature = 68F
- ☐ Minimum Pipe Size Local Street Single Family Residential, 6-inch
- Water Demands (as outlined in "Water System Demands")

See "Water System Demands" (Appendix 1)



Hydraulic Model

Modeling Methodology

The software design package selected for electronic modeling is WaterCad v5.0.

The output data calculated by the electronic model is:

- Schematic Model
- □ Fire Flow Report (total flow needed, total flow available, minimum & residual pressures, etc.)
- ☐ Junction Report (pressures, demand outflow, etc.)
- □ Pipe Report (line sizes, velocities, etc.)
- □ Reservoir Report (inflow, HG, etc.)

See Appendix 2. Hydraulic Model Output Data

Conclusions

The data supplied by the model demonstrates that the designed system design represents an adequately sized system for the assumptions as listed herein.



MERRILL RANCH - PULTE DEVELOPMENT WEST OF FELIX ROAD WATER SYSTEM DEMANDS 10/19/2004

					Wate	Water Systen Demands	spt						Equalization
	:		-	Residential			Commercia	sial			Total		Storage
Parcel		do d	Ave. Day	Peak Day	Day	Average Day) Day	Peak Day	Day	Ave. Day	Peak Day	Day	Gallons
	#	pers	pd6	pdb	mdb	acre	pd6	pdb	mdg	pd6	pdb	mdb	(48% Peak Day)
-	98	155	15,500	31,000	22	0	0	0	0	15,500	31,000	22	14,880
2	137	356	35,599	71,198	49	0	0	0	0	35,599	71,198	49	34,175
ဗ	106	191	19,115	38,231	27	0	0	0	0	19,115	38,231	23	18,351
4	102	266	26,579	53,159	28	0	0	0	0	26,579	53,159	37	25,516
5	118	212	21,151	42,303	59	0	0	0	0	21,151	42,303	58	20,305
9	141	368	36,779	73,557	51	0	0	0	0	36,779	73,557	51	35,307
7	75	135	13,464	26,929	19	0	0	0	0	13,464	26,929	19	12,926
8	125	325	32,498	64,996	45	0	0	0	0	32,498	64,996	45	31,198
6	117	210	21,046	42,092	29	0	0	0	0	21,046	42,092	29	20,204
10	190	494	49,358	98,717	69	0	0	0	0	49,358	98,717	69	47,384
11	88	158	15,830	31,660	22	0	0	0	0	15,830	31,660	22	15,197
12	119	311	31,067	62,135	43	0	0	0	0	31,067	62,135	43	29,825
13	142	255	25,483	50,965	32	0	0	0	0	25,483	50,965	38	24,463
14	20	129	12,886	25,771	18	0	0	0	0	12,886	25,771	18	12,370
15	63	114	11,372	22,745	16	0	0	0	0	11,372	22,745	16	10,918
16	119	309	30,904	61,807	43	0	0	0	0	30,904	61,807	43	29,667
17	103	185	18,505	37,009	26	0	0	0	0	18,505	37,009	26	17,765
18	82	214	21,392	42,785	30	0	0	0	0	21,392	42,785	30	20,537
19	75	134	13,415	26,830	19	0	0	0	0	13,415	26,830	19	12,879
20	181	472	47,174	94,349	99	0	0	0	0	47,174	94,349	99	45,287
21	98	177	17,662	35,325	25	0	0	0	0	17,662	35,325	25	16,956
22	135	351	35,053	70,106	49	0	0	0	0	35,053	70,106	49	33,651
23	133	240	23,973	47,947	33	0	0	0	0	23,973	47,947	33	23,014
24	115	300	30,008	60,016	42	0	0	0	0	30,008	60,016	42	28,808
25	82	147	14,672	29,344	20	0	0	0	0	14,672	29,344	20	14,085
26	06	235	23,456	46,912	33	0	0	0	0	23,456	46,912	33	22,518
27	91	165	16,469	32,938	23	0	0	0	0	16,469	32,938	23	15,810
28	133	345	34,474	68,949	48	0	0	0	0	34,474	68,949	48	33,095
29	91	163	16,343	32,685	23	0	0	0	0	16,343	32,685	23	15,689
30	126	328	32,847	65,695	46	0	0	0	0	32,847	65,695	46	31,533
31	135	243	24,275	48,550	34	0	0	0	0	24,275	48,550	34	23,304

MERRILL RANCH - PULTE DEVELOPMENT WEST OF FELIX ROAD WATER SYSTEM DEMANDS 10/19/2004

Equalization	Storage	Gallons	(48% Peak Day)	38,578	21,882	83,425	22,239	39,480	19,645	83,163	18,230	13,883	16,646	16,848	21,485	12,198	33,790	24,989	26,593	20,757	4.267
		Day	mdb	56	32	121	35	22	88	120	26	20	24	24	31	18	49	36	38	30	9
	Total	Peak Day	pd6	80,371	45,588	173,803	46,332	82,249	40,927	173,257	37,978	28,922	34,679	35,100	44,760	25,412	70,397	52,060	55,402	43,243	8.891
		Ave. Day	pdb	40,186	22,794	86,901	23,166	41,125	20,463	86,628	18,989	14,461	17,339	17,550	22,380	12,706	35,198	26,030	27,701	21,622	4 445
		Day	mdb	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	ial	Peak Day	pd6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	c
ds	Commercial	Day	pd6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Water Systen Demands		Average Day	acre	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Water		Day	mdg	56	32	121	32	57	28	120	56	20	24	24	31	18	49	36	38	30	9
	Residential	Peak Day	pd6	80,371	45,588	173,803	46,332	82,249	40,927	173,257	37,978	28,922	34,679	35,100	44,760	25,412	70,397	52,060	55,402	43,243	8 891
	Œ	Ave. Day	pd6	40,186	22,794	86,901	23,166	41,125	20,463	86,628	18,989	14,461	17,339	17,550	22,380	12,706	35,198	26,030	27,701	21,622	4.445
		Рор	pers	402	228	698	232	411	205	998	190	145	173	176	224	127	352	260	277	312	64
	-	D. U.	#	155	127	334	129	158	114	333	105	80	96	98	124	71	196	145	154	120	25
		Parcel		32	33	34	35	36	37	38	33	41	43	45	47	49	51	53	55	A	8

MERRILL RANCH - PULTE DEVELOPMENT WEST OF FELIX ROAD WATER SYSTEM DEMANDS 10/19/2004

					Wate	Water Systen Demands	spu						Equalization
	:	,	<u></u>	Residential			Commercial	ial			Total		Storage
Parcel		rop	Ave. Day	Peak Day	Day	Average Day	Day	Peak Day	Day	Ave. Day	Peak Day	Day	Gallons
	#	pers	pd6	pd6	md6	acre	pdb	pd6	mdb	pd6	pd6	mdb	(48% Peak Day)
ပ	0	0	0	0	0	22.56	33,840	089'29	47	33,840	67,680	47	32,486
۵	0	0	0	0	0	12.01	18,015	36,030	25	18,015	36,030	25	17,294
Ш	0	0	0	0	0	6.92	10,380	20,760	14	10,380	20,760	14	9,965
L	0	0	0	0	0	10	15,000	30,000	21	15,000	30,000	21	14,400
ტ	0	0	0	0	0	18	27,000	54,000	88	27,000	54,000	88	25,920
I	0	0	0	0	0	12.02	18,030	36,060	25	18,030	36,060	25	17,309
	0	0	0	0	0	0.5	750	1,500	1	750	1,500	1	720
ſ	0	0	0	0	0	0.5	750	1,500	_	750	1,500		720
¥	0	0	0	0	0	2	3,000	000'9	4	3,000	9,000	4	2,880
٦	0	0	0	0	0	17.03	25,545	51,090	35	25,545	51,090	35	24,523
M	0	0	0	0	0	55.86	83,790	167,580	116	83,790	167,580	116	80,438
Z	0	0	0	0	0	1.54	2,310	4,620	3	2,310	4,620	3	2,218
0	0	0	0	0	0	16	24,000	48,000	33	24,000	48,000	33	23,040
Ъ	0	0	0	0	0	5.63	8,445	16,890	12	8,445	16,890	12	8,107
σ	0	0	0	0	0	1.96	2,940	5,880	4	2,940	5,880	4	2,822
ж	0	0	0	0	0	18.04	27,060	54,120	38	27,060	54,120	38	25,978
Totals	6,011	13,196	1,308,037	2,616,075	1,817	201	300,855	601,710	418	1,608,892	3,217,785	2,235	1,544,537
					•					Fire Suppr	Fire Suppression Storage (gal):	age (gal):	120,000
											Total Storage (gal):	age (gal):	1,664,537

Water System Design Criteria:

gpd per person (residentail areas requiring sewers)

persons/D.U. (all Family Community Residences)

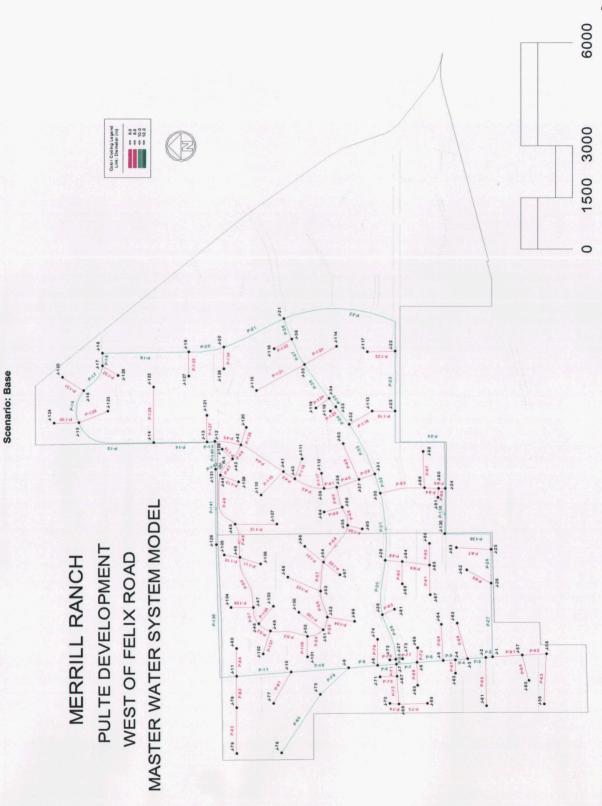
persons/D.U. (all Active Adult Community Residences)

gpd per acre (all commercial and school areas) 100 2.6 1.8 1,500 2.0

peak day factor (average day multiplier)

Note that all calculations are based on "Johnson Utilities Company Design Guide and Standard Details" May 2003.

File: 742 WATER DEMANDS-JU 10-18-04.xls Page: 3 of 3 Printed: 10/19/2004



Title: ANTHEM @ MERRILL RANCH y:\...\watercad\742 master water 11-1-04.wcd 11/03/04 02:32:14 PM

Jack Johnson Company © Haestad Methods, Inc. 37 Brookside Road Waterbury, CT 06708 USA +1-203-755-1666

Scenario: Base **Fire Flow Analysis Fire Flow Report**

Label	Needed Fire Flow (gpm)	Total Flow Needed (gpm)	Total Flow Available (gpm)	Residual Pressure (psi)	Calculated M Residual Pressure (psi)	finimum Syster Pressure (psi)	Calculated Minimum System Pressure (psi)	Minimum System Junction	Fire Flow Balanced?	Satisfies Fire Flow Constraints?
J-1	1,000	1,000	2,645	20.00	34.10	20.00	20.00	J-76	true	true
J-2	1,000	1,000	2,638	20.00	32.27	20.00	20.00	J-76	true	true
J-3	1,000	1,000	2,619	20.00	33.22	20.00	20.00	J-76	true	true
J-4	1,000	1,000	2,605	20.00	31.83	20.00	20.00	J-76	true	true
J-5	1,000	1,000	2,591	20.00	30.45	20.00	20.00	t e	true	true
J-6	1,000	1,000	2,554	20.00	32.47	20.00	20.00		true	true
J-7	1,000	1,000	2,519	20.00	31.80	20.00	20.00	ł.	true	true
J-8	1,000	1,000	2,469	20.00	31.20	20.00	20.00	l.	true	true
J-9	1,000	1,000	2,393	20.00	33.03	20.00	20.00		true	true
J-10	1,000	1,000	2,581	20.00	28.18	20.00	20.00		true	true
J-11	1,000	1,000	2,749	20.00	28.74	20.00	20.00		true	true
J-12	1,000	1,000	5,000	20.00	28.85	20.00	20.43		true	true
J-13	1,000	1,000	4,644	20.00	27.50	20.00	20.00 20.00		true	true
J-14	1,000	1,000	3,173	20.00	26.56 24.32	20.00 20.00	20.00		true	true
J-15 J-16	1,000 1,000	1,000	2,355	20.00 20.00	24.32 24.31	20.00	20.00	1	true	true
J-10 J-17	1,000	1,000	2,181 2,053	20.00	22.16	20.00	20.00		true	true
J-17 J-18	1,000	1,000 1,000	2,053	20.00	20.00	20.00	20.00		true true	true
J-19	1,000	1,000	1,830	20.00	21.18	20.00	20.99		true	true true
J-19 J-20	1,000	1,000	1,757	20.00	21.10	20.00	20.00		true	true
J-20 J-21	1,000	1,000	1,645	20.00	20.00	20.00		J-116	true	true
J-22	1,000	1,000	1,663	20.00	22.19	20.00		J-117	true	true
J-23	1,000	1,000	1,681	20.00	25.90	20.00	20.00		true	true
J-24	1,000	1,000	1,693	20.00	24.93	20.00	20.00		true	true
J-25	1,000	1,000	2,630	20.00	27.13	20.00	20.00		true	true
J-26	1,000	1,000	2,649	20.00	26.63	20.00	20.00	ł .	true	true
J-27	1,000	1,000	2,535	20.00	30.81	20.00	20.00		true	true
J-28	1,000	1,000	2,641	20.00	28.23	20.00	20.00		true	true
J-29	1,000	1,000	2,667	20.00	27.39	20.00		J-115	true	true
J-30	1,000	1,000	1,718	20.00	25.18	20.00	20.00	J-115	true	true
J-31	1,000	1,000	1,724	20.00	25.72	20.00	20.00	J-115	true	true
J-32	1,000	1,000	1,667	20.00	22.56	20.00	20.00	J-115	true	true
J-33	1,000	1,000	1,637	20.00	22.71	20.00	20.00	J-115	true	true
J-34	1,000	1,000	1,622	20.00	22.90	20.00	20.00	J-115	true	true
J-35	1,000	1,000	1,568	20.00	26.07	20.00	20.00	J-115	true	true
J-36	1,000	1,000	1,619	20.00	20.44	20.00	20.00	J-116	true	true
J-37	1,000	1,000	1,795	20.00	22.62	20.00	20.00	J-115	true	true
J-38	1,000	1,000	1,909	20.00	21.80	20.00	20.00	J-115	true	true
J-39	1,000	1,000	1,912	20.00	22.16	20.00	20.00	J-112	true	true
J-40	1,000	1,000	1,916	20.00	22.17	20.00	20.00	J-111	true	true
J-41	1,000	1,000	2,032	20.00	21.03	20.00		J-111	true	true
J-42	1,000	1,000	2,600	20.00	20.03	20.00		J-109	true	true
J-43	1,000	1,000	1,954	20.00	20.00	20.00		J-109	true	true
J-44	1,000	1,000	1,706	20.00	20.00	20.00		J-108	true	true
J-45	1,000	1,000	1,299	20.00	20.01	20.00		J-107	true	true
J-46	1,000	1,000	1,530	20.00	20.00	20.00		J-106	true	true
J-47	1,000	1,000	1,386	20.00	24.47	20.00		J-102	true	true
J-48	1,000	1,000	1,345	20.00	23.41	20.00		J-102	true	true
J-49	1,000	1,000	1,315	20.00	24.33	20.00		J-102	true	true
J-50	1,000	1,000	1,396	20.00	21.18	20.00		J-102	true	true
J-51	1,000	1,000	1,436	20.00	20.00	20.00		J-102	true	true
J-52	1,000	1,000	1,474	20.00	23.35	20.00	20.00	J-51	true	true

Scenario: Base Fire Flow Analysis Fire Flow Report

Label	Needed Fire Flow (gpm)	Total Flow Needed (gpm)	Total Flow Available (gpm)	Residual Pressure (psi)	Calculated M Residual Pressure (psi)	/linimum Systen Pressure (psi)	n Calculated Minimum System Pressure (psi)	Minimum System Junction	Fire Flow Balanced?	Satisfies Fire Flow Constraints?
J-53	1,000	1,000	1,555	20.00	21.89	20.00	20.00	J-102	true	true
J-54	1,000	1,000	1,625	20.00	22.17	20.00	20.00	J-96	true	true
J-55	1,000	1,000	1,469	20.00	20.01	20.00	20.00	J-95	true	true
J-56	1,000	1,000	1,673	20.00	20.01	20.00	20.00	J-95	true	true
J-57	1,000	1,000	2,078	20.00	22.17	20.00	20.00	J-60	true	true
J-58	1,000	1,000	1,756	20.00	22.22	20.00	20.00	J-59	true	true
J-59	1,000	1,066	1,408	20.00	20.00	20.00	33.82	J-21	true	true
J-60	1,000	1,030	1,723	20.00	20.00	20.00		J-21	true	true
J-61	1,000	1,043	1,729	20.00	20.00	20.00	30.76		true	true
J-62	1,000	1,042	2,014	20.00	20.00	20.00	27.90	J-76	true	true
J-63	1,000	1,018	2,462	20.00	20.00	20.00		J-76	true	true
J-64	1,000	1,049	2,047	20.00	20.00	20.00		J-76	true	true
J-65	1,000	1,038	2,242	20.00	20.00	20.00		J-76	true	true
J-66	1,000	1,025	2,492	20.00	20.00	20.00		J-76	true	true
J-67	1,000	1,000	2,406	20.00	20.04	20.00		J-70	true	true
J-68	1,000	1,000	1,730	20.00	20.00	20.00	20.00		true	true
J-69	1,000	1,043	1,511	20.00	20.00	20.00	28.46		true	true
J-70	1,000	1,025	1,637	20.00	20.00	20.00	23.94		true	true
J-71	1,000	1,021	1,963	20.00	20.00	20.00	27.41	J-76	true	true
J-72	1,000	1,001	2,536	20.00	24.93	20.00	20.00	J-76	true	true
J-73	1,000	1,001	2,536	20.00	24.72	20.00		J-76	true	true
J-74	1,000	1,047	2,134	20.00	20.00	20.00	25.12		true	true
J-75	1,000	1,069	1,888	20.00	28.67	20.00	20.00		true	true
J-76	1,000	1,045	1,427	20.00	20.00	20.00	34.46		true	true
J-77	1,000	1,051	1,658	20.00	20.00	20.00		J-76	true	true
J-78	1,000	1,037	1,594	20.00	24.36	20.00		J-79	true	true
J-79	1,000	1,049	1,145	20.00	20.00	20.00		J-78	true	true
J-80	1,000	1,022	2,029	20.00	20.00	20.00	29.11	J-79	true	true
J-81	1,000	1,004	2,473	20.00	20.00	20.00	22.18		true	true
J-82	1,000	1,048	2,042	20.00	20.00	20.00	27.35		true	true
J-83	1,000	1,046	1,923	20.00	20.00	20.00	28.43	J-21	true	true
J-84	1,000	1,000	2,131	20.00	24.36	20.00	20.00	J-86	true	true
J-85 J-86	1,000	1,000	1,646	20.00 20.00	22.17 20.00	20.00 20.00	20.00 29.90	J-86 J-85	true	true
J-87	1,000 1,000	1,033 1,033	1,468 1,545	20.00	20.00	20.00	29.90		true	true
J-88	1,000	1,035	1,870	20.00	20.00	20.00	28.12		true true	true
J-89	1,000	1,000	1,701	20.00	23.31	20.00	20.00		true	true true
J-90	1,000	1,000	1,696	20.00	24.22	20.00	20.00		true	true
J-91	1,000	1,003	1,698	20.00	20.00	20.00	20.03		true	true
J-92	1,000	1,056	1,377	20.00	20.00	20.00	27.32		true	true
J-93	1,000	1,032	1,334	20.00	20.00	20.00	28.90		true	true
J-94	1,000	1,023	1,498	20.00	20.00	20.00	26.93		true	true
J-95	1,000	1,023	1,388	20.00	20.00	20.00	24.73	i	true	true
J-96	1,000	1,026	1,426	20.00	20.00	20.00		J-102	true	true
J-97	1,000	1,016	1,494	20.00	20.00	20.00		J-102	true	true
J-98	1,000	1,019	1,339	20.00	20.00	20.00		J-102	true	true
J-99	1,000	1,035	1,372	20.00	20.00	20.00		J-102	true	true
J-100	1,000	1,022	1,341	20.00	20.00	20.00		J-102	true	true
J-101	1,000	1,022	1,304	20.00	20.00	20.00		J-102	true	true
J-102	1,000	1,029	1,189	20.00	20.00	20.00	30.20		true	true
J-103	1,000	1,019	1,287	20.00	20.00	20.00		J-102	true	true
J-103	1,000	1,019	1,308	20.00	20.00	20.00		J-102 J-102	true	true

Scenario: Base **Fire Flow Analysis Fire Flow Report**

Label	Needed Fire Flow (gpm)	Total Flow Needed (gpm)	Total Flow Available (gpm)	Residual Pressure (psi)	Calculated I Residual Pressure (psi)	linimum Syster Pressure (psi)	n Calculated Minimum System Pressure (psi)	Minimum System Junction	Fire Flow Balanced?	Satisfies Fire Flow Constraints?
J-105	1,000	1,020	1,410	20.00	20.00	20.00	24.69	J-102	true	true
J-106	1,000	1,025	1,372	20.00	20.00	20.00	26.02	J-102	true	true
J-107	1,000	1,033	1,138	20.00	20.00	20.00	29.29	J-45	true	true
J-108	1,000	1,023	1,501	20.00	20.00	20.00	27.17	J-44	true	true
J-109	1,000	1,014	1,689	20.00	20.00	20.00	26.58	J-43	true	true
J-110	1,000	1,030	1,550	20.00	20.00	20.00	30.27	J-21	true	true
J-111	1,000	1,030	1,583	20.00	20.00	20.00	28.94	J-21	true	true
J-112	1,000	1,006	1,661	20.00	20.00	20.00	25.44	J-21	true	true
J-113	1,000	1,121	1,811	20.00	23.69	20.00	20.00	J-115	true	true
J-114	1,000	1,120	1,308	20.00	20.00	20.00	28.38	J-115	true	true
J-115	1,000	1,028	1,078	20.00	20.00	20.00	31.58	J-21	true	true
J-116	1,000	1,032	1,364	20.00	20.00	20.00	26.43	J-115	true	true
J-117	1,000	1,057	1,351	20.00	20.00	20.00	27.40	J-21	true	true
J-118	1,000	1,012	1,497	20.00	20.00	20.00	23.05	J-115	true	true
J-119	1,000	1,004	1,641	20.00	20.54	20.00	20.00	J-115	true	true
J-120	1,000	1,026	1,950	20.00	20.00	20.00	30.05	J-21	true	true
J-121	1,000	1,024	2,290	20.00	20.00	20.00	35.83	J-18	true	true
J-122	1,000	1,031	1,451	20.00	20.00	20.00	36.72	J-18	true	true
J-123	1,000	1,049	1,683	20.00	20.00	20.00	29.98	J-18	true	true
J-124	1,000	1,036	1,792	20.00	20.00	20.00	28.45	J-18	true	true
J-125	1,000	1,038	1,638	20.00	20.00	20.00	28.71	J-18	true	true
J-126	1,000	1,018	1,682	20.00	20.00	20.00	26.31	J-18	true	true
J-127	1,000	1,024	1,458	20.00	20.00	20.00	27.18	J-21	true	true
J-128	1,000	1,020	1,449	20.00	20.00	20.00	26.24	J-21	true	true
J-129	1,000	1,000	4,431	20.00	30.45	20.00	20.00	J-79	true	true
J-130	1,000	1,000	2,598	20.00	24.60	20.00	20.00	J-21	true	true
J-131	1,000	1,000	5,000	20.00	48.45	20.00	38.05	J-21	true	true

Scenario: Base **Steady State Analysis Junction Report**

Label	Elevation (ft)	Туре	Base Flow (gpm)	Demand (Calculated) (gpm)	Calculated Hydraulic Grade (ft)	Pressure Head (ft)	Pressure (psi)
J-1	1,455.00	Demand	0	0	1,611.77	156.77	67.83
J-2	1,460.00		l ol	0	1,611.77	151.77	65.66
J-3	1,460.00		o	0	1,611.79	151.79	65.67
J-4		Demand	lol	0	1,611.82	146.82	63.52
J-5		Demand	o	0	1,611.85	141.85	61.37
J-6	1,470.00		0	0	1,611.95	141.95	61.41
J-7		Demand	ا ا	ō	1,612.07	136.07	58.87
J-8	1,480.00		اً و	0	1,612.32	132.32	57.25
J-9		Demand	0	o	1,612.79	132.79	57.45
J-10		Demand	اً و	0	1,614.13	124.13	53.71
J-11	1,490.00		ا	0	1,615.60	125.60	54.34
J-12	1,500.00		ا	o	1,620.99	120.99	52.35
J-12 J-13	· ·	Demand		0	1,620.76	120.76	52.35 52.25
J-13 J-14		Demand		0	1,619.24	119.24	52.25 51.59
J-14 J-15	1,505.00			o		112.03	
					1,617.03		48.47
J-16	1,505.00			0	1,616.34	111.34	48.17
J-17	1,510.00				1,615.76	105.76	45.76
J-18	1,515.00		0	0	1,615.54	100.54	43.50
J-19	1,510.00		0	0	1,614.10	104.10	45.04
J-20	1,510.00		0	0	1,613.55	103.55	44.80
J-21	1,513.00		0	0	1,612.59	99.59	43.09
J-22	1,500.00		이	0	1,612.10	112.10	48.50
J-23	1,490.00		이	0	1,611.99	121.99	52.78
J-24	1,485.00		이	0	1,611.88	126.88	54.89
J-25	1,470.00	Demand	0	0	1,611.78	141.78	61.34
J-26	1,470.00		이	0	1,611.77	141.77	61.34
J-27	1,476.00	Demand	이	0	1,612.07	136.07	58.87
J-28	1,467.00	Demand		0	1,612.02	145.02	62.74
J-29	1,465.00	Demand	이	0	1,611.96	146.96	63.58
J-30	1,488.00	Demand	0	0	1,611.98	123.98	53.64
J-31	1,490.00	Demand	0	0	1,612.01	122.01	52.79
J-32	1,500.00	Demand	0	o	1,612.01	112.01	48.46
J-33	1,500.00	Demand	0	0	1,612.03	112.03	48.47
J-34	1,500.00	Demand	0	0	1,612.04	112.04	48.48
J-35	1,496.00	Demand	o	0	1,612.09	116.09	50.23
J-36	1,509.00	Demand	0	0	1,612.34	103.34	44.71
J-37	1,491.00	Demand	0	o	1,612.10	121.10	52.40
J-38	1,485.00	Demand	0	o	1,612.32	127.32	55.09
J-39	1,485.00		0	o	1,612.72	127.72	55.26
J-40	1,490.00		0	o	1,613.72	123.72	53.53
J-41	1,490.00		l ol	o	1,614.27	124.27	53.77
J-42	1,500.00		o	o	1,616.66	116.66	50.47
J-43	1,500.00		0	o	1,616.05	116.05	50.21
J-44	1,490.00		0	o	1,615.37	125.37	54.24
J-45	1,480.00		o o	o	1,613.81	133.81	57.89
J-46	1,480.00	İ	0	ő	1,613.09	133.09	57.58
J-47	1,475.00			ő	1,612.38	137.38	57.56 59.44
J-48	1,480.00			ő	1,612.21	132.21	59.44 57.20
J-46 J-49	1,480.00		0				
			I I	0	1,612.12	132.12	57.16 57.00
J-50	1,480.00		0	0	1,611.96	131.96	57.09
J-51	1,480.00		0	0	1,611.93	131.93	57.08
J-52	1,470.00		0	0	1,611.92	141.92	61.40
J-53	1,470.00		0	0	1,611.92	141.92	61.40
J-54	1,470.00	Demand	0	0	1,611.93	141.93	61.4

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Scenario: Base **Steady State Analysis Junction Report**

Label	Elevation (ft)	Туре	Base Flow (gpm)	Demand (Calculated) (gpm)	Calculated Hydraulic Grade (ft)	Pressure Head (ft)	Pressure (psi)
J-55	1,480.00	Demand	0	0,	1,612.04	132.04	57.13
J-56	1,480.00	Demand	lol	o	1,612.15	132.15	57.17
J-57	1,455.00		lol	o	1,611.61	156.61	67.76
J-58	1,450.00	Demand	l ol	0	1,611.55	161.55	69.89
J-59	1,455.00	Demand	66	66	1,611.41	156.41	67.67
J-60	1,460.00	Demand	30	30	1,611.59	151.59	65.59
J-61	1,470.00	Demand	43	43	1,611.71	141.71	61.31
J-62	1,460.00	Demand	42	42	1,611.75	151.75	65.65
J-63	1,470.00	Demand	18	18	1,611.81	141.81	61.36
J-64	1,460.00	Demand	49	49	1,611.79	151.79	65.67
J-65	1,470.00	Demand	38	38	1,611.93	141.93	61.40
J-66	1,470.00	Demand	25	25	1,611.94	141.94	61.41
J-67	1,480.00	Demand	l ol	ol	1,612.01	132.01	57.12
J-68	1,480.00	Demand	lol	o	1,611.94	131.94	57.08
J-69	1,475.00	Demand	43	43	1,611.90	136.90	59.23
J-70			25	25	1,611.93	131.93	57.08
J-71		Demand	21	21	1,612.01	132.01	57.11
J-72	1,476.00	Demand	1	1	1,612.07	136.07	58.87
J-73	1,475.00		1	1	1,612.07	137.07	59.30
J-74	,	Demand	47	47	1,612.29	137.29	59.40
J-75	·		69	69	1,612.69	122.69	53.08
J-76	1,510.00		45	45	1,612.66	102.66	44.4
J-77	1,500.00		51	51	1,614.07	114.07	49.3
J-78	1,500.00		37	37	1,615.46	115.46	49.9
J-79	1,510.00		49	49	1,615.39	105.39	45.60
J-80	1,490.00		22	22	1,615.59	125.59	54.3
J-81	1,465.00		4	4	1,612.02	147.02	63.6°
J-82	-	Demand	48	48	1,611.73	141.73	61.3
J-83	1,470.00		46	46	1,611.73	141.73	61.3
J-84	•	Demand	o	ol	1,611.86	146.86	63.5
J-85	•	Demand	o	ő	1,611.79	141.79	61.3
J-86	1,475.00		33	33	1,611.78	136.78	59.1
J-87	1,460.00		33	33	1,611.77	151.77	65.6
J-88	,	Demand	35	35	1,611.85	146.85	63.5
J-89	1,485.00	Demand	0	o	1,611.88	126.88	54.8
J-90	1,485.00	Demand	ا	ő	1,611.88	126.88	54.8
J-91	1,485.00		3	3	1,611.88	126.88	54.8
J-92	1,490.00		56	56	1,611.81	121.81	52.7
J-93	1,497.00		32	32	1,612.08	115.08	49.7
J-94	1,480.00		23	23	1,612.14	132.14	57.1
J-95	1,480.00		34	34	1,612.03	132.03	57.1
J-96	1,475.00		26	26	1,611.92	136.92	59.2
J-97	1,470.00		16	16	1,611.93	141.93	61.4
J-98	1,470.00		19	19	1,611.91	141.91	61.4
J-99	1,470.00		35	35	1,611.90	141.90	61.3
J-100	1,470.00		22	22	1,611.92	141.92	61.4
J-100 J-101	1,480.00	l	29	29	1,611.95	131.95	57.0
J-101 J-102	1,490.00		29	29	1,612.10	122.10	52.8
J-102	1,480.00		19	19	1,612.21	132.21	57.2
J-103 J-104	1,480.00		27	27	1,612.21	132.37	57.2 57.2
J-104 J-105	1,480.00		20	20	1,613.09	133.09	57.2 57.5
J-105 J-106	1,480.00		25	20 25	1,613.09	133.08	57.5 57.5
J-106 J-107	1,480.00	1	33	33	1,613.78	133.78	57.5 57.8
U-1U/	1,400.00	Pelligila	23	23	1,615.37	125.37	57.8 54.2

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Project Engineer: Seth Wallace

ster 11-1-04.wcd Jack Johnson Company
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Scenario: Base Steady State Analysis Junction Report

Label	Elevation (ft)	Туре	Base Flow (gpm)	Demand (Calculated) (gpm)	Calculated Hydraulic Grade (ft)	Pressure Head (ft)	Pressure (psi)
J-109	1,500.00	Demand	14	14	1,616.05	116.05	50.21
J-110	1,490.00	Demand	30	30	1,614.25	124.25	53.76
J-111	1,495.00	Demand	30	30	1,613.70	118.70	51.36
J-112	1,490.00	Demand	6	6	1,612.72	122.72	53.10
J-113	1,490.00	Demand	121	121	1,611.94	121.94	52.76
J-114	1,505.00	Demand	120	120	1,611.80	106.80	46.21
J-115	1,510.00	Demand	28	28	1,612.06	102.06	44.16
J-116	1,510.00	Demand	32	32	1,612.33	102.33	44.27
J-117	1,505.00	Demand	57	57	1,612.05	107.05	46.31
J-118	1,500.00	Demand	12	12	1,612.04	112.04	48.47
J-119	1,498.00	Demand	4	4	1,612.03	114.03	49.34
J-120	1,500.00	Demand	26	26	1,616.65	116.65	50.47
J-121	1,505.00	Demand	24	24	1,620.75	115.75	50.08
J-122	1,510.00	Demand	31	31	1,619.20	109.20	47.25
J-123	1,505.00	Demand	49	49	1,616.98	111.98	48.45
J-124	1,505.00	Demand	36	36	1,617.01	112.01	48.46
J-125	1,510.00	Demand	38	38	1,616.32	106.32	46.00
J-126	1,510.00	Demand	18	18	1,615.76	105.76	45.76
J-127	1,510.00	Demand	24	24	1,614.09	104.09	45.03
J-128	1,510.00	Demand	20	20	1,613.54	103.54	44.80
J-129	1,485.00	Demand	o	0	1,620.93	135.93	58.81
J-130	1,480.00	Demand	o	0	1,611.84	131.84	57.04
J-131	1,500.00	Demand	o	0	1,623.63	123.63	53.49

Scenario: Base **Steady State Analysis Pipe Report**

Label	Length (ft)	Diameter (in)	Material	Hazen- Williams C	Check Valve?	Control Status	Discharge (gpm)	Headloss Gradient (ft/1000ft)	Pressure Pipe Headloss (ft)	Velocity (ft/s)
P-2	203.00	12.0	PVC	150.0	false	Open	-82	0.02	0.00	0.23
P-3	518.00	12.0	PVC	150.0	false	Open	-125	0.04	0.02	0.35
P-4	367.00	12.0	PVC	150.0	false	Open	-167	0.07	0.03	0.47
P-5	341.00	12.0	PVC	150.0	false	Open	-185	0.09	0.03	0.52
P-6	760.00	12.0	PVC	150.0	false	Open	-234	0.13	0.10	0.66
P-7	604.00	12.0	PVC	150.0	false	Open	-297	0.20	0.12	0.84
P-8	544.00	12.0	PVC	150.0	false	Open	-460	0.46	0.25	1.31
P-9	837.00	12.0	PVC	150.0	false	Open	-507	0.55	0.46	1.44
P-10	1,674.00	12.0	PVC	150.0	false	Open	-621	0.81	1.35	1.76
P-11	1,571.00	12.0		150.0	false	Open	-672	0.93	1.46	1.91
P-13	224.00	12.0	PVC	150.0	false	Open	717	1.05	0.24	2.03
P-14	1,545.00		PVC	150.0	false	Open	693	0.99	1.52	1.97
P-15	2,435.00	12.0	PVC	150.0	false	Open	662	0.91	2.21	1.88
P-16	983.00	12.0	PVC	150.0	false	Open	577	0.70	0.69	1.64
P-17	931.00	12.0	PVC	150.0	false	Open	539	0.62	0.58	1.53
P-18	375.00	12.0	PVC	150.0	false	Open	521	0.58	0.22	1.48
P-19	2,492.00	12.0		150.0	false	Open	521	0.58	1.45	1.48
P-21	1,939.00	12.0		150.0	false	Open	477	0.49	0.96	1.35
P-22	4,177.00	12.0	PVC	150.0	false	Open	218	0.12	0.49	0.62
P-23	1,726.00	12.0	PVC	150.0	false	Open	161	0.07	0.11	0.46
P-24	3,667.00	12.0	PVC	150.0	false	Open	106	0.03	0.11	0.30
P-26	981.00	12.0	PVC	150.0	false	Open	62	0.01	0.01	0.18
P-27	2,131.00	12.0	PVC	150.0	false	Open	14	0.00	0.00	0.04
P-28	147.00	10.0		150.0	false	Open	74	0.04	0.01	0.30
P-29 P-30	1,365.00 1,589.00	10.0	PVC PVC	150.0	false	Open	72	0.04	0.05	0.30
P-31	1,956.00	10.0	PVC	150.0 150.0	false true	Open Open	68	0.03 0.01	0.05 0.02	0.28 0.13
P-32	582.00	10.0	PVC	150.0	false	Open	-94	0.01	0.02	0.13
P-33	1,614.00	10.0	PVC	150.0	false	Open	3	0.00	0.00	0.01
P-34	637.00		PVC	150.0	false	Open	-63	0.03	0.02	0.26
P-35	322.00		PVC	150.0	false	Open	-67	0.03	0.02	0.27
P-36	1,209.00	10.0		150.0	false	Open	-79	0.04	0.05	0.32
P-37	823.00	10.0	PVC	150.0	false	Open	-227	0.30	0.25	0.93
P-38	639.00	10.0	PVC	150.0	false	Open	-259	0.39	0.25	1.06
P-39	477.00	8.0	PVC	150.0	false	Open	-97	0.19	0.09	0.62
P-40	690.00		PVC	150.0	false	Open	-129	0.31	0.22	0.82
P-41	378.00	8.0	PVC	150.0	false	Open	-249	1.07	0.40	1.59
P-42	887.00		PVC	150.0	false	Open	-255	1.12	0.99	1.63
P-43	401.00	8.0		150.0	false	Open	-285	1.38	0.55	1.82
P-44	1,447.00	8.0		150.0	false	Open	-315	1.65	2.39	2.01
P-45	761.00	8.0	PVC	150.0	false	Open	-615	5.69	4.33	3.92
P-46	481.00	8.0	PVC	150.0	false	Open	273	1.27	0.61	1.74
P-47	590.00		PVC	150.0	false	Open	259	1.15	0.68	1.65
P-48	1,612.00	8.0	PVC	150.0	false	Open	236	0.97	1.56	1.51
P-49	986.00	8.0	PVC	150.0	true	Open	203	0.73	0.72	1.30
P-50	1,532.00	8.0	PVC	150.0	false	Open	158	0.46	0.71	1.01
P-51	526.00	8.0	PVC	150.0	false	Open	131	0.33	0.17	0.84
P-52	400.00	8.0	PVC	150.0	false	Open	112	0.24	0.10	0.72
P-53	1,077.00		PVC	150.0	false	Open	83	0.14	0.15	0.53
P-54	506.00		PVC	150.0	false	Open	54	0.06	0.03	0.35
P-55	401.00		PVC	150.0	false	Open	32	0.02	0.01	0.21
P-56	769.00	8.0	PVC	150.0	false	Open	-3	0.00	0.00	0.02
P-57	855.00	8.0	PVC	150.0	false	Open	-22	0.01	0.01	0.14

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Scenario: Base **Steady State Analysis Pipe Report**

P-58	abel	Length (ft)	Diameter (in)	Material	Hazen- Williams C	Check Valve?	Control Status	Discharge (gpm)	Headloss Gradient (ft/1000ft)	Pressure Pipe Headloss (ft)	Velocity (ft/s)
P-60 613.00 8.0 PVC 150.0 false Open 96 0.8 P-61 855.00 8.0 PVC 150.0 false Open 96 0.18 P-62 691.00 8.0 PVC 150.0 false Open 66 0.09 P-64 756.00 8.0 PVC 150.0 false Open 43 0.04 P-65 1,415.00 8.0 PVC 150.0 false Open 43 0.04 P-66 1,094.00 8.0 PVC 150.0 false Open 42 0.04 P-67 337.00 8.0 PVC 150.0 false Open 49 0.05 P-69 663.00 8.0 PVC 150.0 false Open 38 0.01 P-71 422.00 8.0 PVC 150.0 false Open 25 0.02 P-71 356.00 8.0 <td< td=""><td>58</td><td>1,301.00</td><td>8.0</td><td>PVC</td><td>150.0</td><td>true</td><td>Open</td><td>64</td><td>0.09</td><td>0.11</td><td>0.41</td></td<>	58	1,301.00	8.0	PVC	150.0	true	Open	64	0.09	0.11	0.41
P-81 855.00 8.0 PVC 150.0 false Open 66 0.18 P-62 691.00 8.0 PVC 150.0 false Open 66 0.09 P-84 756.00 8.0 PVC 150.0 false Open 66 0.09 P-84 756.00 8.0 PVC 150.0 false Open 43 0.04 P-65 1.415.00 8.0 PVC 150.0 false Open 43 0.04 P-66 1.084.00 8.0 PVC 150.0 false Open 42 0.04 P-87 387.00 8.0 PVC 150.0 false Open 42 0.04 P-88 1.065.00 8.0 PVC 150.0 false Open 42 0.05 P-89 683.00 8.0 PVC 150.0 false Open 49 0.05 P-89 683.00 8.0 PVC 150.0 false Open 49 0.05 P-70 422.00 8.0 PVC 150.0 false Open 38 0.03 P-70 422.00 8.0 PVC 150.0 false Open 89 0.16 P-72 809.00 8.0 PVC 150.0 false Open 89 0.16 P-73 816.00 8.0 PVC 150.0 false Open 43 0.04 P-74 221.00 8.0 PVC 150.0 false Open 68 0.10 P-75 488.00 8.0 PVC 150.0 false Open 43 0.04 P-76 173.00 8.0 PVC 150.0 false Open 43 0.04 P-76 173.00 8.0 PVC 150.0 false Open 43 0.04 P-76 173.00 8.0 PVC 150.0 false Open 43 0.04 P-77 192.00 8.0 PVC 150.0 false Open 43 0.04 P-77 192.00 8.0 PVC 150.0 false Open 43 0.04 P-78 173.00 8.0 PVC 150.0 false Open 43 0.04 P-78 173.00 8.0 PVC 150.0 false Open 44 0.00 P-79 1.124.00 10.0 PVC 150.0 false Open 10 0.00 P-79 1.124.00 10.0 PVC 150.0 false Open 47 0.05 P-88 90.00 8.0 PVC 150.0 false Open 47 0.05 P-88 90.00 8.0 PVC 150.0 false Open 47 0.05 P-88 90.00 8.0 PVC 150.0 false Open 47 0.05 P-88 90.00 8.0 PVC 150.0 false Open 47 0.05 P-88 90.00 8.0 PVC 150.0 false Open 45 0.02 P-88 90.00 8.0 PVC 150.0 false Open 45 0.02 P-88 90.00 8.0 PVC 150.0 false Open 45 0.02 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-89 98.00 8.0 PVC 150.0 false Open 46 0.05 P-99 147.00 8.0 PVC 150.0 false Open 46 0.05 P-99 147.00 8.0 PVC 150.0 false Open 46 0.05 P-99 147.00 8.0 PVC 150.0 false Open 46 0.05 Open 47 0.00 P-99 147.00 8.0 PVC 150.0 false Open 33 0.03 0.03 P-99 147.00 8.0 PVC 150.0 false Open 35 0.03 P-99 147.00 8.0 PVC 150.0 false Open 35 0.03 P-99 147.00 8.0 PVC 150.0 false Open 35 0.03 P-99	59	551.00	8.0	PVC	150.0	false	Open	-98	0.19	0.10	0.62
P-62	30	613.00	8.0	PVC	150.0	false	Open	-121	0.28	0.17	0.77
P-83	31	855.00	8.0	PVC	150.0	false	Open	96	0.18	0.16	0.61
P-84	32	691.00	8.0	PVC	150.0	false	Open	66	0.09	0.06	0.42
P-84	sa	1,464.00	8.0	PVC	150.0	false	Open	66	0.09	0.13	0.42
P-86	64		8.0	PVC	150.0	false	Open	30	0.02	0.02	0.19
P-66	35	1,415.00	8.0	PVC		false	Open	i I	0.04	0.06	0.27
P-67 387.00 8.0 PVC 150.0 false Open 49 0.05 P-68 63.00 8.0 PVC 150.0 false Open 49 0.05 P-70 422.00 8.0 PVC 150.0 false Open 25 0.02 P-71 356.00 8.0 PVC 150.0 false Open 25 0.02 P-71 356.00 8.0 PVC 150.0 false Open 89 0.16 P-72 809.00 8.0 PVC 150.0 false Open 68 0.10 P-73 816.00 8.0 PVC 150.0 false Open 43 0.04 P-74 261.00 8.0 PVC 150.0 false Open 25 0.01 P-75 488.00 8.0 PVC 150.0 false Open 25 0.01 P-76 173.00 8.0 PVC 150.0 false Open 25 0.01 P-77 192.00 8.0 PVC 150.0 false Open 21 0.01 P-78 763.00 8.0 PVC 150.0 false Open 1 0.00 P-79 1,124.00 10.0 PVC 150.0 false Open 47 0.05 P-80 2,038.00 10.0 PVC 150.0 false Open 47 0.05 P-81 1,039.00 8.0 PVC 150.0 false Open 45 0.02 P-82 907.00 8.0 PVC 150.0 false Open 45 0.02 P-84 794.00 8.0 PVC 150.0 false Open 49 0.05 P-85 382.00 8.0 PVC 150.0 false Open 49 0.05 P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 49 0.05 P-88 494.00 8.0 PVC 150.0 false Open 48 0.05 P-89 627.00 8.0 PVC 150.0 false Open 46 0.05 P-89 627.00 8.0 PVC 150.0 false Open 46 0.05 P-89 627.00 8.0 PVC 150.0 false Open 46 0.05 P-89 627.00 8.0 PVC 150.0 false Open 46 0.05 P-99 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PVC 150.0 false Open 30 0.03 P-91 847.00 8.0 PV				I						0.04	0.2
P-88			8.0	PVC		false	1		1	0.00	0.1
P-89 663.00 8.0 PVC 150.0 false Open 38 0.03 P-70 422.00 8.0 PVC 150.0 false Open 25 0.02 P-71 356.00 8.0 PVC 150.0 false Open 89 0.16 P-72 809.00 8.0 PVC 150.0 false Open 68 0.10 P-73 816.00 8.0 PVC 150.0 false Open 43 0.04 P-74 261.00 8.0 PVC 150.0 false Open 43 0.04 P-75 488.00 8.0 PVC 150.0 false Open 25 0.01 Open P-76 488.00 8.0 PVC 150.0 false Open 25 0.01 Open P-77 192.00 8.0 PVC 150.0 false Open 1 0.00 Open P-78 763.00 8.0 PVC 150.0 false Open 1 0.00 Open P-79 1,124.00 10.0 PVC 150.0 false Open 47 0.05 Open P-81 1,039.00 8.0 PVC 150.0 false Open 45 0.02 Open P-84 794.00 8.0 PVC 150.0 false Open 45 0.02 Open 51 0.06 Open 45 0.02 Open 45 0.02 Open 45 0.05 Open							· ·	l I		0.06	0.3
P-70				I -			l '		·	0.02	0.24
P-71 356.00 8.0 PVC 150.0 false Open 89 0.16 P-72 809.00 8.0 PVC 150.0 false Open 68 0.10 P-73 816.00 8.0 PVC 150.0 false Open 68 0.10 P-74 261.00 8.0 PVC 150.0 false Open 25 0.01 P-75 488.00 8.0 PVC 150.0 false Open 25 0.01 P-76 173.00 8.0 PVC 150.0 false Open 21 0.01 P-77 192.00 8.0 PVC 150.0 false Open 1 0.00 P-78 763.00 8.0 PVC 150.0 false Open 1 0.00 P-79 1,124.00 10.0 PVC 150.0 false Open 47 0.05 P-80 2,038.00 10.0 PVC 150.0 false Open 114 0.08 P-81 1,039.00 8.0 PVC 150.0 false Open 47 0.05 P-82 907.00 8.0 PVC 150.0 false Open 45 0.02 P-83 1,344.00 8.0 PVC 150.0 false Open 45 0.02 P-84 794.00 8.0 PVC 150.0 false Open 45 0.02 P-85 382.00 8.0 PVC 150.0 false Open 49 0.05 P-86 806.00 8.0 PVC 150.0 false Open 49 0.05 P-87 998.00 8.0 PVC 150.0 false Open 48 0.05 P-88 494.00 8.0 PVC 150.0 false Open 46 0.05 P-89 787.00 8.0 PVC 150.0 false Open 46 0.05 P-89 627.00 8.0 PVC 150.0 false Open 46 0.05 P-991 847.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 35 0.03 P-991 847.00 8.0 PVC 150.0 false Open 32 0.03 P-993 1,297.00 8.0 PVC 150.0 false Open 32 0.03 P-994 401.00 8.0 PVC 150.0 false Open 32 0.02 P-995 187.00 8.0 PVC 150.0 false Open 32 0.03 P-996 138.00 PVC 150.0 false Open 32 0.03 P-997 1,051.00 8.0 PVC 150.0 false Open 34 0.03 P-910 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 32 0.02 P-102 599.00 8.0 PVC 150.0 false Open 34 0.03 P-103 426.0	i i			I			1 '	I I	1	0.01	0.10
P-72	i i	ſ		1	, ,		l '			0.06	0.1
P-73					1		· .			0.08	0.3
P-74					1			i I		0.03	0.4
P-75				_	1		· .			0.00	0.1
P-76					1					0.00	0.1
P-77	1			_	1		· .	l			
P-78	1				1		i '	l l		0.00	0.0
P-79	1			-	1		L	· ·		0.00	0.0
P-80				-	1		'	l I		0.04	0.3
2-81 1,039.00 8.0 PVC 150.0 false Open 51 0.08 2-82 907.00 8.0 PVC 150.0 false Open 86 0.15 2-83 1,344.00 8.0 PVC 150.0 false Open 49 0.05 2-84 794.00 8.0 PVC 150.0 false Open 22 0.01 2-85 382.00 8.0 PVC 150.0 false Open 48 0.05 2-86 806.00 8.0 PVC 150.0 false Open 48 0.05 2-87 998.00 8.0 PVC 150.0 false Open 46 0.05 2-88 494.00 8.0 PVC 150.0 false Open 33 0.03 2-91 847.00 8.0 PVC 150.0 false Open 33 0.03 2-91 847.00 8.0 <td< td=""><td>ì</td><td>· .</td><td></td><td></td><td>1</td><td></td><td>· ·</td><td></td><td></td><td>0.10</td><td>0.4</td></td<>	ì	· .			1		· ·			0.10	0.4
P-82 907.00 8.0 PVC 150.0 false Open 86 0.15 P-83 1,344.00 8.0 PVC 150.0 false Open 49 0.05 P-84 794.00 8.0 PVC 150.0 false Open 22 0.01 P-85 382.00 8.0 PVC 150.0 false Open 48 0.05 P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 46 0.05 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 66 0.09 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 61 0.08 P-95 187.00 8.0 PVC 150.0 false Open 5 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 5 0.00 P-99 1,138.00 8.0 PVC 150.0 false Open 5 0.00 P-99 542.00 8.0 PVC 150.0 false Open 50.00 P-99 542.00 8.0 PVC 150.0 false Open 32 0.02 P-101 704.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 35 0.01 P-101 704.00 8.0 PVC 150.0 false Open 36 0.02 P-102 599.00 8.0 PVC 150.0 false Open 36 0.02 P-103 1,044.00 8.0 PVC 150.0 false Open 36 0.02 P-104 806.00 8.0 PVC 150.0 false Open 36 0.02 P-105 862.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 36 0.02 P-106 601.00 8.0 PVC 150.0 false Open 39 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-109 643.00 8.0 PVC 150.0 false Open 29 0.02 P-109 643.00 8.0 PVC 150.0 false Open 29 0.02 P-109 643.00 8.0 PVC 150.0 false Open 29 0.02				_	1		I '			0.03	0.1
P-83 1,344.00 8.0 PVC 150.0 false Open 49 0.05 P-84 794.00 8.0 PVC 150.0 false Open 22 0.01 P-85 382.00 8.0 PVC 150.0 false Open 4 0.00 P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 101 0.20 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 <td< td=""><td>1</td><td></td><td></td><td></td><td>1</td><td></td><td>i '</td><td>l i</td><td></td><td>0.06</td><td>0.3</td></td<>	1				1		i '	l i		0.06	0.3
P-84 794.00 8.0 PVC 150.0 false Open 22 0.01 P-85 382.00 8.0 PVC 150.0 false Open 4 0.00 P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 66 0.09 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 5 0.03 P-93 1,297.00 8.0 PVC					1 1		1 '	i i		0.14	0.5
P-85 382.00 8.0 PVC 150.0 false Open 4 0.00 P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 66 0.09 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 5 0.03 P-94 401.00 8.0 PVC					1		1 '	1	l l	0.07	0.3
P-86 806.00 8.0 PVC 150.0 false Open 48 0.05 P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 101 0.20 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 P					1 1	false	Open	1		0.01	0.1
P-87 998.00 8.0 PVC 150.0 false Open 46 0.05 P-88 494.00 8.0 PVC 150.0 false Open 101 0.20 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0	35		8.0	PVC		false	Open		0.00	0.00	0.0
P-88 494.00 8.0 PVC 150.0 false Open 101 0.20 P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 <td< td=""><td>36</td><td></td><td>8.0</td><td>PVC</td><td></td><td>false</td><td>Open</td><td>48</td><td>· · · · · · · · · · · · · · · · · · ·</td><td>0.04</td><td>0.3</td></td<>	36		8.0	PVC		false	Open	48	· · · · · · · · · · · · · · · · · · ·	0.04	0.3
P-89 787.00 8.0 PVC 150.0 false Open 66 0.09 P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 32 0.02 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 <td< td=""><td>37</td><td>998.00</td><td>8.0</td><td>I -</td><td>150.0</td><td>false</td><td>Open</td><td>46</td><td>0.05</td><td>0.05</td><td>0.2</td></td<>	37	998.00	8.0	I -	150.0	false	Open	46	0.05	0.05	0.2
P-90 627.00 8.0 PVC 150.0 false Open 33 0.03 P-91 847.00 8.0 PVC 150.0 false Open 33 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 22 0.00 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 <t< td=""><td>38</td><td>494.00</td><td>8.0</td><td>PVC</td><td>150.0</td><td>false</td><td>Open</td><td>101</td><td>0.20</td><td>0.10</td><td>0.6</td></t<>	38	494.00	8.0	PVC	150.0	false	Open	101	0.20	0.10	0.6
P-91 847.00 8.0 PVC 150.0 false Open 35 0.03 P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 32 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 29 0.02 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 27 0.02	39	787.00	8.0	PVC	150.0	false	Open	66	0.09	0.07	0.4
P-92 646.00 8.0 PVC 150.0 false Open 35 0.03 P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0	90	627.00	8.0	PVC	150.0	false	Open	33	0.03	0.02	0.2
P-93 1,297.00 8.0 PVC 150.0 false Open 61 0.08 P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0	91	847.00	8.0	PVC	150.0	false	Open	33	0.03	0.02	0.2
P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0	92	646.00	8.0	PVC	150.0	false	Open	35	0.03	0.02	0.2
P-94 401.00 8.0 PVC 150.0 false Open 5 0.00 P-95 187.00 8.0 PVC 150.0 false Open 2 0.00 P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0	93	1,297.00	8.0	PVC	150.0	false	Open	61	0.08	0.10	0.3
P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0	94		8.0	PVC	1 1		1	5		0.00	0.0
P-97 1,051.00 8.0 PVC 150.0 false Open 56 0.07 P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0	95	187.00	8.0	PVC	150.0	false	Open		0.00	0.00	0.0
P-98 1,138.00 8.0 PVC 150.0 false Open 32 0.02 P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0	97	l l	8.0	PVC		false	Open			0.07	0.3
P-99 542.00 8.0 PVC 150.0 false Open 23 0.01 P-100 425.00 8.0 PVC 150.0 false Open 34 0.03 P-101 704.00 8.0 PVC 150.0 false Open 26 0.02 P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0	98	1,138.00				false				0.03	0.2
P-100		1					3			0.01	0.1
P-101							1	I I		0.01	0.2
P-102 599.00 8.0 PVC 150.0 false Open 16 0.01 P-103 1,044.00 8.0 PVC 150.0 false Open 19 0.01 P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 19 0.01 P-109 643.00 8.0 PVC 150.0 false Open 27 0.02							1	i i		0.01	0.1
P-103					l I		1 -	1	1	0.00	0.1
P-104 806.00 8.0 PVC 150.0 false Open 35 0.03 P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 19 0.01 P-109 643.00 8.0 PVC 150.0 false Open 27 0.02					1 1					0.01	0.1
P-105 862.00 8.0 PVC 150.0 false Open 22 0.01 P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 19 0.01 P-109 643.00 8.0 PVC 150.0 false Open 27 0.02										0.02	0.2
P-106 601.00 8.0 PVC 150.0 false Open 29 0.02 P-107 703.00 8.0 PVC 150.0 false Open 29 0.02 P-108 660.00 8.0 PVC 150.0 false Open 19 0.01 P-109 643.00 8.0 PVC 150.0 false Open 27 0.02										0.02	0.2
P-107				•			1 '			0.01	0. 0.
P-108 660.00 8.0 PVC 150.0 false Open 19 0.01 0.02				l							
P-109 643.00 8.0 PVC 150.0 false Open 27 0.02	j			l						0.01	0.1
										0.01	0.1
D 440 I 40400I 0 0 DVO I 4500 I I O I 00 I 00 I				l			1			0.01	0.1
P-110 464.00 8.0 PVC 150.0 false Open 20 0.01 P-111 632.00 8.0 PVC 150.0 false Open 25 0.02				l	1		1 '	3		0.00 0.01	0.1 0.1

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Jack Johnson Company

Project Engineer: Seth Wallace WaterCAD v5.0 [5.0037]

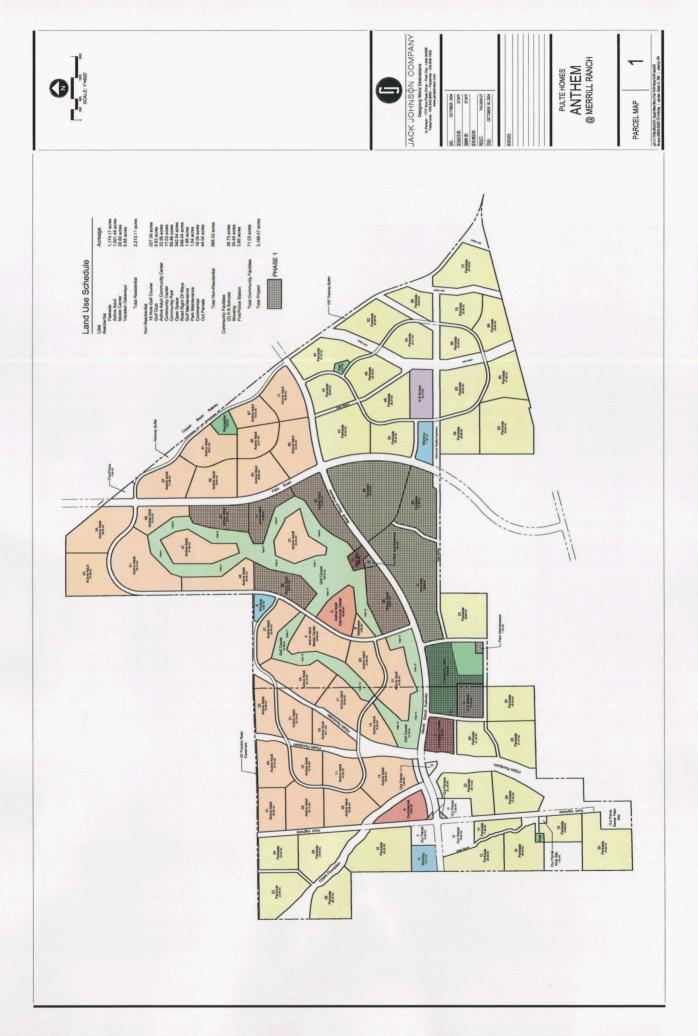
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Scenario: Base **Steady State Analysis** Pipe Report

Label	Length (ft)	Diameter (in)	Material	Hazen- Williams C	Check Valve?	Control Status	Discharge (gpm)	Headloss Gradient (ft/1000ft)	Pressure Pipe Headloss (ft)	Velocity (ft/s)
P-112	1,205.00	8.0	PVC	150.0	false	Open	33	0.03	0.03	0.21
P-113	557.00	8.0	PVC	150.0	false	Open	23	0.01	0.01	0.15
P-114	411.00	8.0	PVC	150.0	false	Open	14	0.01	0.00	0.09
P-115	955.00	8.0	PVC	150.0	false	Open	30	0.02	0.02	0.19
P-116	625.00	8.0	PVC	150.0	false	Open	30	0.02	0.01	0.19
P-117	436.00	8.0	PVC	150.0	false	Open	6	0.00	0.00	0.04
P-118	770.00	8.0	PVC	150.0	false	Open	66	0.09	0.07	0.42
P-119	674.00	8.0	PVC	150.0	false	Open	-55	0.07	0.04	0.35
P-120	1,059.00	8.0	PVC	150.0	false	Open	120	0.28	0.29	0.77
P-121	1,593.00	8.0	PVC	150.0	false	Open	28	0.02	0.03	0.18
P-122	582.00	8.0	PVC	150.0	false	Open	32	0.02	0.01	0.20
P-123	799.00	8.0	PVC	150.0	false	Open	57	0.07	0.06	0.36
P-124	482.00	8.0	PVC	150.0	false	Open	12	0.00	0.00	0.08
P-125	200.00	8.0	PVC	150.0	false	Open	4	0.00	0.00	0.03
P-126	530.00	8.0	PVC	150.0	false	Open	26	0.02	0.01	0.17
P-127	770.00	8.0	PVC	150.0	false	Open	24	0.01	0.01	0.15
P-128	1,615.00	8.0	PVC	150.0	false	Open	31	0.02	0.04	0.20
P-129	902.00	8.0	PVC	150.0	false	Open	49	0.05	0.05	0.31
P-130	717.00	8.0	PVC	150.0	false	Open	36	0.03	0.02	0.23
P-131	719.00	8.0	PVC	150.0	false	Open	38	0.03	0.02	0.24
P-132	534.00	8.0	PVC	150.0	false	Open	18	0.01	0.00	0.11
P-133	694.00	8.0	PVC	150.0	false	Open	24	0.01	0.01	0.15
P-134	624.00	8.0	PVC	150.0	false	Open	20	0.01	0.01	0.13
P-136	4,342.00	12.0	PVC	150.0	false	Open	-780	1.23	5.33	2.21
P-139	1,765.00	12.0	PVC	150.0	false	Open	108	0.03	0.06	0.31
P-96	264.00	8.0	PVC	150.0	false	Open	3	0.00	0.00	0.02
P-138	1,317.00	12.0	PVC	150.0	true	Open	108	0.03	0.04	0.31
P-20	1,032.00	12.0	PVC	150.0	false	Open	497	0.53	0.55	1.41
P-140	796.00	12.0	PVC	150.0	false	Open	-1,332	3.31	2.63	3.78
P-141	2,196.00	12.0	PVC	150.0	true	Open	780	1.23	2.70	2.21
P-142	177.00	12.0	PVC	150.0	false	Open	2,112	7.76	1.37	5.99

Scenario: Base **Steady State Analysis Reservoir Report**

Label	Elevation (ft)	Zone	Inflow (gpm)	Calculated Hydraulic Grade (ft)
R-1	1,625.00	Zone-1	-2,112	1,625.00





JACK JOHNSON COMPANY

Designing World Destinations

In-Person -- 1777 Sun Peak Drive - Park City - Utah 84098 Telephone - 435.645 9000 -- Facsimile - 435.649 1620

ATTACHMENT 4

JOHNSON UTILITIES Aquatic Consulting & Testing Laboratory Reports for Wells

Source	Date	Nitrate Result	Date	Arsenic Result
Oasis POE001	9/14/2004	1.02	6/16/2003	0.022
Skyline POE001	9/14/2004	6.92	8/20/2003	0.003
Johnson Ranch POE001	8/11/2004	8.83	6/18/1997	0.005
Sun Valley 5 POE001	8/24/2004	0.57	6/5/2004	0.005
Circle Cross POE001	8/31/2004	0.96	11/5/2003	0.002
Wildhorse POE001	9/14/2004	8.45	3/31/2004	< 0.005

ATTACHMENT 5

JOHNSON UTILITIES IDENTIFICATION NUMBERS FOR ALL DRINKING WATER SYSTEMS

System Number

Johnson Utilities Water System	11-128		
Sun Valley Water System	11-116		
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ATTACHMENT 6

JOHNSON UTILITIES FACILITY NUMBERS FOR ALL WASTEWATER TREATMENT PLANTS

ld Number	Facility	
103081	SECTION 11	
105004	PRECISION	
105324	PECAN RECLAMATION PLANT	
105325	SANTAN RECLAMATION PLANT	